



DELAWARE RIVER BASIN BLAIR CREEK, WARREN COUNTY NEW JERSEY

# BLAIR LAKE DAM NJ 00774

PHASE 1 INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM



#### DEPARTMENT OF THE ARMY

Philadelphia District Corps of Engineers Philadelphia, Pennsylvania

REPT. NO! DAEN | NAP-53842 | NJO 0774-81/08

AUGUST 1981

81 9 05 040

SECURITY CLASSIFICATION OF THIS PAGE (When Dete Entered) READ INSTRUCTIONS REPORT DOCUMENTATION PAGE BEFORE COMPLETING FORM 2. GOVT ACCESSION NO. 3. RECIPIENT'S CATALOG NUMBER DAEN/NAP#53842/NJ00774-81/08 TYPE OF REPORT & PERIOD COVERED TITLE (and Subtitle) Phase I Inspection Report .... National Dam Safety Program. Blair Lake Dam (NJ00774), S. PERFORNING ONG. REPORT NUMBER Warren County, New Jersey, · AUTHOR(+) 6. CONTRACT OR GRANT NUMBER(4) /DACW61-79-C-0011 Guinan, Warren, P.E./ 10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS 9. PERFORMING ORGANIZATION NAME AND ADDRESS Anderson-Nichols 150 Causeway St Boston, MA 02114 1. CONTROLLING OFFICE NAME AND ADDRESS NJ Department of Environmental Protection Division of Water Resources 12. REPORT DATE Auguss, 1981 13. NUMBER OF PAGES P.O. Box CN029 Trenton, NJ 08625
18. MONITORING AGENCY NAME & ADDRESS(II different from Controlling Office) 15. SECURITY CLASS. (of this report) U.S. Army Engineer District, Philadelphia Custom House, 2d & Chestnut Streets Unclassified Philadelphia, PA 19106 15a. DECLASSIFICATION/DOWNGRADING 16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited. 17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report) 18. SUPPLEMENTARY NOTES Copies are obtainable from National Technical Information Service, Springfield, Virginia 22151. 19. KEY WORDS (Continue on reverse side if necessary and identify by block number) National Dam Safety Program Embankments Blair Lake Dam, NJ00774 Visual Inspection **Spillways** Structural Analysis Seepage ABSTRACT (Couchum as reverse side M respecting and ideality by block market) This report cites results of a technical investigation as to the dam's adequacy. The inspection and evaluation of the dam is as prescribed by the National Dam Inspection Act, Public Law 92-367. The technical investigation includes visual inspection, review of available design and construction records, and preliminary structural and hydraulic and hydrologic calculations, as applicable. An assessment of the dam's general condition is included in the report.

DO 1 JAN 73 1473 EDITION OF 1 NOV 65 IS OBSOLETE

SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered)



# DEPARTMENT OF THE ARMY PHILADELPHIA DISTRICT, CORPS OF ENGINEERS CUSTOM HOUSE - 2 D & CHESTNUT STREETS PHILADELPHIA, PENNSYLVANIA 19106

IN REPLY HEFER TO

NAPEN-N

3 1 AUG 1981

Accession For
PTIS GRA&I
DTIC TAB
Unannounced
Justification

By\_\_\_\_
Distribution/

Availability Joseph

Dist

Avoil and/or

Specia

Honorable Brendan T. Byrne Governor of New Jersey Trenton, New Jersey 08621

Dear Governor Byrne:

Inclosed is the Phase I Inspection Report for Blair Lake Dam in Warren County, New Jersey which has been prepared under authorization of the Dam Inspection Act, Public Law 92-367. A brief assessment of the dam's condition is given in the front of the report.

Based on visual inspection, available records, calculations and past operational performance, Blair Lake Dam, a high hazard potential structure, is judged to be in fair overall condition. The spillway is considered seriously inadequate since a flow equivalent to 5 percent of the Probable Maximum Flood (PMF) would cause the dam to be overtopped. The seriously inadequate spillway is assessed as an UNSAFE, non-emergency condition, until more detailed studies prove otherwise or corrective measures are completed. The classification of UNSAFE applied to a dam because of a seriously inadequate spillway is not meant to indicate the same degree of emergency as would be associated with an UNSAFE classification applied for a structural deficiency. It does mean, however, that based on an initial screening, and preliminary computations, there appears to be a serious deficiency in spillway capacity so that if a severe storm were to occur, overtopping and failure of the dam could take place, significantly increasing the hazard of loss of life downstream from the dam. To ensure adequacy of the structure, the following actions, as a minimum, are recommended.

a. The spillway's adequacy should be determined by a qualified professional consultant engaged by the owner using more sophisticated methods, procedures and studies within six months from the date of approval

APPROVED FOR PUBLIC RELEASE; DISTRIBUTION UNLIMITED.

#### NAPEN-N

Honorable Brendan T. Byrne

of this report. Within three months of the consultant's findings remedial measures to ensure spillway adequacy should be initiated. In the interim, a detailed emergency operation plan and warning system should be promptly developed. Also, during periods of unusually heavy precipitation, around the clock surveillance should be provided.

- b. Within six months of the date of approval of this report the owner should engage a qualified professional consultant to perform the following:
- (1) Design and oversee installation of a properly sized low-level outlet and gate.
- (2) Design and oversee procedures for the removal of trees and root systems from immediately upstream and downstream of the dam.
- (3) Evaluate the potential for undermining of the abutment support at the right side of the dam owing to the loss of several large bedrock blocks.
- (4) Design and oversee procedures for elimination of the seepage through the stone masonry in the spillway.
- (5) Design and oversee repair or replacement to the service bridge trusses and wood deck.
- c. The owner should develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam, within one year from the date of approval of this report.

A copy of the report is being furnished to Mr. Dirk C. Hofman, New Jersey Department of Environmental Protection, the designated State Office contact for this program. Within five days of the date of this letter, a copy will also be sent to Congressman Courter of the Thirteenth District. Under the provision of the Freedom of Information Act, the inspection report will be subject to release by this office, upon request, five days after the date of this letter.

Additional copies of this report may be obtained from the National Technical Information Services (NTIS), Springfield, Virginia 22161 at a reasonable cost. Please allow four to six weeks from the date of this letter for NTIS to have copies of the report available.

NAPEN-N

Honorable Brendan T. Byrne

An important aspect of the Dam Inspection Program will be the implementation of the recommendations made as a result of the inspection. We accordingly request that we be advised of proposed actions taken by the State to implement our recommendations.

Sincerely,

Incl

As stated

ROGER L. BALDWIN

Lieutenant Colonel, Corps of Engineers Commander and District Engineer

Copies furnished:

Mr. Dirk C. Hofman, P.E., Deputy Director Division of Water Resources N.J. Dept. of Environmental Protection P.O. Box CN029 Trenton, NJ 08625

Mr. John O'Dowd, Acting Chief Bureau of Flood Plain Regulation Division of Water Resources N.J. Dept. of Environmental Protection P.O. Box CN029 Trenton, NJ 08625

#### BLAIR LAKE DAM (NJUU774)

#### CORPS OF ENGINEERS ASSESSMENT OF GENERAL CONDITIONS

This dam was inspected on 22 April 1981 by Anderson-Nichols & Co., Inc. under contract to the State of New Jersey. The State, under agreement with the U.S. Army Engineer District, Philadelphia, had this inspection performed in accordance with the National Dam Inspection Act, Public Law 92-367.

Blair Lake Dam, a high hazard potential structure, is judged to be in fair overall condition. The spillway is considered seriously inadequate since a flow equivalent to 5 percent of the Probable Maximum Flood (PMF) would cause the dam to be overtopped. The seriously inadequate spillway is assessed as an UNSAFE, non-emergency condition, until more detailed studies prove otherwise or corrective measures are completed. The classification of UNSAFE applied to a dam because of a seriously inadequate spillway is not meant to indicate the same degree of emergency as would be associated with an UNSAFE classification applied for a structural deficiency. It does mean, however, that based on an initial screening, and preliminary computations, there appears to be a serious deficiency in spillway capacity so that if a severe storm were to occur, overtopping and failure of the dam could take place, significantly increasing the hazard of loss of life downstream from the dam. To ensure adequacy of the structure, the following actions, as a minimum, are recommended.

- a. The spillway's adequacy should be determined by a qualified professional consultant engaged by the owner using more sophisticated methods, procedures and studies within six months from the date of approval of this report. Within three months of the consultant's findings remedial measures to ensure spillway adequacy should be initiated. In the interim, a detailed emergency operation plan and warning system should be promptly developed. Also, during periods of unusually heavy precipitation, around the clock surveillance should be provided.
- b. Within six months of the date of approval of this report the owner should engage a qualified professional consultant to perform the following:
- (1) Design and oversee installation of a properly sized low-level outlet and gate.
- (2) Design and oversee procedures for the removal of trees and root systems from immediately upstream and downstream of the dam.
- (3) Evaluate the potential for undermining of the abutment support at the right side of the dam owing to the loss of several large bedrock blocks.
- (4) Design and oversee procedures for elimination of the seepage through the stone masonry in the spillway.
- (5) Design and oversee repair or replacement to the service bridge trusses and wood deck.

c. The owner should develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam, within one year from the date of approval of this report.

APPROVED:

ROGER L. BALDWIN

Lieutenant Colonel, Corps of Engineers

Commander and District Engineer

DATE:

.

## PHASE I INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM

Name of Dam: Identification No.: State Located:

State Located: County Located: Stream: River Basin: Date of Inspection Blair Lake

Fed ID No. NJ00774

New Jersey Warren Blair Creek Delaware

April 22, 1981

#### ASSESSMENT OF GENERAL CONDITIONS

Blair Lake Dam is a 78-year old dam with an ashlar masonry spillway with earthen and bedrock abutments, is 100 feet long and 18.3 feet high, and is in fair condition. It is small in size and has a high hazard classification. Large trees are growing on the abutments and some of their roots have been instrumental, in part, in causing undermining of the bedrocks on the downstream side of the right abutment. Some seepage was observed through the stone masonry of the spillway below the water line near the right and left sides of the spillway. Erosion has exposed tree roots on the right abutment upstream and the left abutment also shows signs of erosion. In 1960 to seal seepage areas, large amounts of clay and lake-bottom sediments were placed in various locations, including along the upstream spillway toe and the left abutment. The service bridge would be a cause for concern should the dam be overtopped. The bridge, whose low chord elevation at the abutments is slightly below that of top of dam, is rusted and corroded. The dam has no low-level outlet as it was built with a mill race to a downstream millbuilding. The old mill race has been filled and the intake gate at the mill appeared to be inoperable.

The spillway is 41 feet long and 4 feet wide. Overtopping or breaching of Blair Lake Dam would cause excessive property damage to the library and Main Street Bridge and probably would result in damage to 4 or 5 houses 300 feet downstream of the Main Street Bridge as well as the loss of 10 to 20 lives. Therefore the dam is classified high hazard.

The spillway is capable of passing 984 cfs at the top of dam or about 4.6 percent of the 21,554 cfs peak inflow from the Probable Maximum Flood (PMF), which is the selected spillway design flood (SDF). The PMF would overtop the dam by 11 feet for up to 15 1/2 hours. The spillway is not capable of passing 50 percent of the 1/2 PMF (10, 777 cfs inflow) without

overtopping (7.6 feet) which would cause failure. (Failure would probably occur with one to two feet of overtopping.) Dam failure resulting from overtopping would significantly increase the hazard to loss of life downstream from the dam from that which would exist just before overtopping failure. The stage would increase from 7.1 feet to 9.8 feet in about 25 minutes upon failure with one foot of overtopping. Therefore, the spillway is considered to be seriously inadequate.

It is recommended that the owner retain the services of a professional engineer, qualified in the design and inspection of dams, to accomplish the following tasks in the near future: investigate the seriously inadequate spillway capacity and implement remedial measures indicated; design and oversee installation of a properly sized low level outlet and gate; Design and oversee procedures for the removal of trees and root systems from immediately downstream of the dam; evaluate the potential for undermining of the abutment support at the right side of the dam owing to the loss of several large bedrock blocks; design and oversee procedures for elimination of the seepage through the stone masonry in the spillway; and design and oversee repair or replacement to the service bridge trusses and wood deck.

It is futher recommended that the owner undertake the following as a part of operating and maintenance procedures starting soon: develop an emergency action plan which outlines actions to be taken by the owner to minimize the downstream effects of an emergency at the dam. In the near future: develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam.

ANDERSON-NICHOLS & COMPANY, INC.

Warren A. Guinan, P.E.

Project Manager

New Jersey No. 16848



#### PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test Flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonable possible storm runoff), or fractions thereof. The test flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

#### CONTENTS

# PHASE I INSPECTION REPORT BLAIR LAKE DAM SAFETY REPORT

#### BLAIR LAKE DAM FED ID NO. NJ00774 NJ NO. 21-11

| SECTION  | 1   | PROJE                | ECT INFORMATION   | Page                  |
|----------|-----|----------------------|---|-----------------------|
| ,        |     | 1.2                  | General Project Description Pertinent Data  | 1<br>1<br>3           |
| SECTION  | 2   | ENGI                 | NEERING DATA  |                       |
|          |     | 2.2                  | Design Construction Operation Evaluation  | 5<br>5<br>5<br>5      |
| SECTION  | 3   | VISU                 | AL INSPECTION   | 6                     |
| SECTION  | 4   | OPERA                | ATIONAL PROCEDURES  |                       |
|          |     | 4.2<br>4.3<br>4.4    | Procedures Maintenance of Dam Maintenance of Operating Facilities Warning System Evaluation of Operational Adequacy | 7<br>7<br>7<br>7<br>7 |
| SECTION  | 5   | HYDRA                | AULIC/HYDROLOGIC  | 8                     |
| SECTION  | 6   | STRUC                | CTURAL STABILITY  | 9                     |
| SECTION  | 7   | ASSES                | SSMENT, RECOMMENDATIONS/REMEDIAL MEASUR   | ES                    |
|          |     | 7.1<br>7.2           | Assessment Recommendations/Remedial Measures  | 10<br>10              |
| FIGURES  |     | 1.                   | Essential Project Features<br>Regional Vicinity Map   |                       |
| APPENDIO | CES | 1.<br>2.<br>3.<br>4. | Check List Visual Inspection Photographs Hydrologic Computations HECl Output References                             |                       |

# PHASE I INSPECTION REPORT NATIONAL DAM SAFETY INSPECTION PROGRAM BLAIR LAKE DAM FED ID NO. #NJ00774

### SECTION 1 PROJECT INFORMATION

#### 1.1 General

- a. Authority. Authority to perform the Phase I Safety Inspection of Blair Lake Dam was received from the State of New Jersey, Department of Environmental Protection, Division of Water Resources by letter dated 12 December 1980 under Basic Contract No. FPM-39 and Contract No. A01093 dated 10 October 1979. This Authority was given pursuant to the National Dam Inspection Act, Public Law 92-367 and by agreement between the State and the U.S. Army Engineers District, Philadelphia. The inspection discussed herein was performed by Anderson-Nichols & Company, Inc.
- b. <u>Purpose</u>: The purpose of the Phase I Investigation is to develop an assessment of the general conditions with respect to the safety of Blair Lake Dam and appurtenances. Conclusions are based upon available data and visual inspection. The results of this study were used to determine any need for emergency measures and to conclude if additional studies, investigations, and analyses are necessary and warranted.

#### 1.2 Project Description

- a. Description of Dam and Appurtenances. Blair Lake Dam is an ashlar stone masonry dam tied to earthen and rock abutments 100 feet long with a hydraulic and structural height of 18.3 feet. The masonry spillway is 41 feet long with a topwidth of 4 feet. On the left (east) side of the spillway is a 39-foot earthen abutment and on the right (west) side is a 20 foot bedrock and earth abutment; both abutments are 4 feet higher than the spillway. The upstream and downstream slopes of the dam are tree-covered and of varying slope. On the right (west) side of the right abutment, extending approximately 200 feet downstream, is the east bank of an old mill race (diversion channel), which provided water power for a flour mill. The mill is no longer operating and the mill gate is assumed inoperable. The mill race has been filled to prevent flow to the mill building.
- b. Location. Blair Lake Dam is located on Blair Creek in Blairstown Township, Warren County, New Jersey. The dam is at 40° 59.0' north latitude 74° 57.6' west longitude on the Blairstown Quadrangle. A location map has been included as Figure 2. The site may be reached by driving on Main Street northward from U.S. Route 94.

- c. Size Classification. Blair Lake Dam is classified as being small in size on the basis of storage at the dam crest of 60 acre-feet, which is less than 1000 acre-feet but more than 50 acre-feet, and on the basis of its height of 18.3 feet, which is less than 40 feet, in accordance with criteria given in the Recommended Guidelines for Safety Inspection of Dams.
- d. Hazard Classification. The potential is present for excessive economic damage to the mill building (now the Catherine Dickson Hofman Public Library), Main Street Bridge, and 4 to 8 houses within 400 to 800 feet downstream of the dam. These structures are built along the rock-wall, lined channel of Blair Brook. With the potential loss of 12 to 20 lives in event of overtopping and/or breach, Blair Lake Dam is classified High Hazard.
- e. Ownership. The dam is owned by the Blair Academy, Mr. J. Ernest Rea, Treasurer of Blairstown Academy, Blairstown, N.J. 07825 can be contacted for information at the above address or by calling (201) 362-6121.
- f. <u>Purpose</u>. Blair Lake Dam was built to provide water power to a flour mill downstream. It is presently used for recreation.
- g. Design and Construction History. Memoirs of Blair, a privately printed document published in 1939 indicates that the dam was built in 1902-03 to provide water power for the flour mill downstream. The memoirs were written by John C. Sharpe, who supervised the reconstruction. Mr. Rea, Treasurer of Blairstown Academy, said that the upstream side of the dam was sealed by Lawrence McConachy Construction Co. in 1960 with 1,500 cubic yards of clay and lake-bottom sediments along the spillway and the left embankment. The old headrace had a concrete cut-off placed in it and backfilled to its present height (See Appendix 2).
- h. Normal Operational Procedure. No operational procedures were found for the dam.
- i. Site Geology. No site specific geologic information (such as borings) was available at the time the dam was inspected. Information derived from the Geologic Map of New Jersey (Kummel and Johnson, 1912) and the Glacial Drift of New Jersey (Salisbury, Kummel, Peet and Whitson, 1902) indicates soils within the immediate site consist of stratified drift which may be comprised of sand and gravel plains, deltas, eskers, kames, and terraces.

Bedrock (massive limestone) was observed in large outcrops at the right side of the downstream channel during inspection. The previously mentioned geologic map indicates that bedrock in this area consists of massive to thin bedded limestone of Cambrian to Ordovician age.

#### 1.3 Pertinent Data

a. Drainage Area

10.85 square miles

b. Discharge at Damsite (cfs)

Maximum flood at damsite - unknown.

Total ungated spillway capacity at maximum pool (top of dam) elevation - 984

c. Elevation (ft. above NGVD)

Top of dam - 359.0

Maximum pool test flood (PMF) - 370

Recreation pool (at time of inspection) - 355

Spillway crest - 355

Streambed at centerline of principal spillway - 340.7

Maximum tailwater (estimated) - 346.5

d. Reservoir (Length in feet)

Maximum pool - 2000 (estimated)

Spillway crest - 700

e. Storage (acre-feet)

Spillway crest - 24

Top of dam - 60

Test flood - (PMF) - 236

f. Reservoir Surface (acres)

Top of dam - 12 (estimated)

Spillway crest - 4.3

#### g. Dam

Type - Ashlar masonry with earth and bedrock abutments

Length - 100 feet

Height - 18.3 feet (hydraulic)

- 18.3 feet (structural)

Top width - 4-foot spillway; varies up to 15 feet on earthen abutments

Side slopes - upstream vertical; downstream 1H:3V (slopes apply to spillway and masonry portion only) slopes on earthen abutment vary.

Zoning - unknown

Impervious core - unknown

Cutoff - unknown

Grout curtain - unknown

#### h. Spillway

Type - Broad crested, Ashler masonry

Length of weir - 41 feet

Crest elevation - 355 feet NGVD

Low level outlet - none present

U/S channel - Blair Lake and Blair Creek

D/S channel - Blair Creek

#### SECTION 2 ENGINEERING DATA

#### 2.1 Design

No hydraulic, hydrologic, or other design engineering data were disclosed.

#### 2.2 Construction

As noted above in Section 1.2.g., Memoirs of Blair indicate that the dam was built in 1902-03 under supervision of Dr. John C. Sharpe and paid for by D.C. Blair, son of John I. Blair, founder of Blairstown, N.J. at a cost of \$15,000. The upstream side of the spillway and left embankment were sealed with 1,500 cubic yards of clay and lake-bottom sediments in about 1960 by Lawrence McConachy Construction Company. Owner's representative stated that a concrete cut-off was placed in the mill's headrace before backfilling to preclude flowing water through the mill. Dampness was causing mildew in the library.

#### 2.3 Operation

No data pertaining to the operation of the dam were found.

#### 2.4 Evaluation

- a. Availability. A search of the New Jersey Department of Environmental Protection files, and contact with community officials revealed a limited amount of information.
- b. Adequacy. The information retrieved is inadequate to evaluate; however, the visual inspection is deemed adequate to complete this Phase I Inspection Report.

#### SECTION 3 VISUAL INSPECTION

#### 3.1 Findings

- a. Dam. The left abutment is eroded. Undermining of some of the large rock outcrops of limestone downstream of the right abutment of the dam has occurred. Trees are growing upstream of the dam at the right and downstream of the dam at both abutments. Evidence of seepage through the masonry joints was noted on both right and left sides of the downstream face of the spillway below the waterline.
- b. Appurtenant Structure. Service bridge: major corrosion of the bottom chord joint gusset plates has substantially reduced the effectiveness of the bridge truss. The wood deck planking is weathered with several planks observed to be deteriorated.
- c. Reservoir Area. The watershed above the lake is gently to moderately sloping, wooded, and is partially urbanized. Some open fields exist along the right side of the reservoir. Slopes on the shore appear to be stable. No evidence of significant sedimentation was observed in the reservoir. However, sediment at the upstream face of the dam reaches nearly to the crest of the spillway. This is the result of the action taken about 1960 to place clay and lake-bottom sediments at the upstream toe of the spillway and left abutment to seal the leaks in the dam.
- d. Downstream Channel. Some erosion and displacement of the vertical masonry block walls along the right and left side of the channels downstream of the dam has occurred. Trees are growing on the left bank of the channel downstream of the spillway. One large tree is leaning into the channel approximately 100 ft downstream of the dam.

## SECTION 4 OPERATIONAL PROCEDURES

#### 4.1 Procedures

No formal operating procedures were disclosed.

#### 4.2 · Maintenance of Dam

No formal maintenance procedures for the dam were found, but from its condition, it is apparent that maintenance is needed to prevent serious deterioration of the structure.

#### 4.3 Maintenance of Operating Facility.

No formal maintenance procedures for the operating facilities were found.

#### 4.4 Warning System

No description of any warning system was disclosed.

#### 4.5 Evaluation of Operational Adequacy

Because of the lack of operation and maintenance procedures, the remedial measures described in Section 7.2 should be implemented as prescribed.

## SECTION 5 HYDROLOGIC/HYDRAULIC

#### 5.1 Evaluation of Features

- a. Design Data. Because no hydrologic or hydraulic data were revealed an evaluation could not be performed.
  - b. Experience Data. No experience data were found.
- c. Visual Observation. The spillway appears to be in good condition. At the left spillway abutment downstream, the bedrock is seriously undermined in part, caused by tree roots that have spread along the joint planes. The dam now has no low-level outlet; the old mill race has been blocked off and the gate in the mill building is closed and presumed to be inoperable. Because the low chord of the bridge is just below top of dam, the condition of the bridge is important in the event of overtopping. The poor structural condition of the trusses, caused by corrosion, makes the bridge a liability to the integrity of the dam if it should collapse.
- d. Blair Lake Overtopping Potential. The hydraulic/hydrologic evaluation for the dam is based on a selected Spillway Design Flood (SDF) equal to the Probable Maximum Flood (PMF) in accordance with the range of test floods given in the evaluation guidelines, for dams classified as High Hazard and small in size. The PMF was determined by application of the SCS dimensionless unit hydrograph to a 24-hour probable maximum precipitation of 22.2 inches. Hydrologic computations are given in Appendix 3. The routed PMF peak discharge for the subject drainage area is 21,554 cfs.

The minimum elevation of the dam allows 2.9 feet of depth above the spillway, before overtopping occurs. Under this head the total spillway capacity is 984 cfs, which is less than the selected SDF inflow (approximately 4.6 percent).

Flood routing calculations indicate that Blair Lake Dam will be overtopped for 15.5 hours to a maximum depth of 11 feet under PMF conditions. It is estimated that the spillway can pass about 4.6 percent of the peak PMF inflow without overtopping the dam.

Bank full condition downstream, which occurs at incipient overtopping, is about 5 to 6 feet. If the dam were to fail at overtopping, a significant increase (3.6 feet) in downstream flood stage would occur at the damage center. Failure with a stage one foot above the dam crest is likely, and would increase the downstream stage by 2.7 feet, causing an increase

to the hazard of loss of life in Blairstown. Since the one-half PMF would overtop the dam by 7.6 feet, more than needed to cause failure, the spillway capacity is seriously inadequate.

e. Drawdown Capability. Since the mill headrace was filled, no drawdown capability has existed at Blair lake Dam.

#### SECTION 6 STRUCTURAL STABILITY.

6.1 Evaluation of Structural Stability. Trees growing immediately upstream of the dam may cause seepage if their root systems penetrate and dislodge the masonry blocks in the dam. Several large blocks of bedrock which have been displaced on the right abutment downstream of the dam may cause stability problems at the right abutment.

Based on visual insection alone, it is not possible to determine the character of the dam foundation or the interior of the cross section. Therefore, it is not possible to evaluate the factor of safety of the dam against slope failure, sliding or overturning.

- 6.2 <u>Design and Construction Data</u>. No design or construction data pertinent to the structural stability of the dam are available.
- 6.3 Operating Records. No operating records pertinent to the structural stability of the dam were available.
- 6.4 Post-Construction Changes. No record of post-construction changes was available; however, Mr. Rea indicated that in about 1960, a total of 1,500 cubic yards of clay and lake-bottom sediments was placed along the upstream toe of the spillway and left embankment.
- 6.5 Seismic Stability. This dam is in Seismic Zone 1. According to the Recommended Guidelines, dams located in Seismic Zone 1 "may be assumed to present no hazard from earthquake provided static stability conditions are satisfactory and conventional safety margins exist." None of the visual observations made during the inspection are indicative of unstable slopes. However, because no data are available concerning the engineering properties of the embankment and foundation materials for this dam, it is not possible to make an engineering evaluation of the stability of the slopes or the factor of safety under static conditions.

## SECTION 7 ASSESSMENT, RECOMMENDATIONS/REMEDIAL MEASURES

#### 7.1 Dam Assessment

- a. Condition. Blair Lake Dam is 78 years old and is in fair condition.
- b. Adequacy of Information. The information available is such that the assessment of the dam must be based primarily on the results of the visual inspection.
- c. <u>Urgency</u>. The recommendations made in 7.2.a and 7.2.b should be implemented by the owner as prescribed.
- d. Necessity for Additional Data/Evaluation. The information available from the visual inspection is adequate to identify the potential problems which are listed in 7.2.a. These problems require the attention of a professional engineer who will have to make additional engineering studies to design or specify remedial measures to rectify the problems. If left unattended, the problems could lead to failure of the dam.

#### 7.2 Recommendations/Remedial Measures

- a. Recommendations. The owner should retain a professional engineer qualified in the design and construction of dams to accomplish the following in the near future:
  - Investigate the seriously inadequate spillway capacity and design, and implement remedial measures indicated.
  - Design and oversee installation of properly sized low-level outlet and gate.
  - 3. Design and oversee procedures for the removal of trees and root systems from immediately upstream and downstream of the dam.
  - 4. Evaluate the potential for undermining of the abutment support at the right side of the dam owing to the loss of several large bedrock blocks.
  - 5. Design and oversee procedures for elimination of the seepage through the stone masonry in the spillway.
  - 6. Design and oversee repair or replacement to the service bridge trusses and wood deck.
  - 7. Consider the provision of a low level outlet.

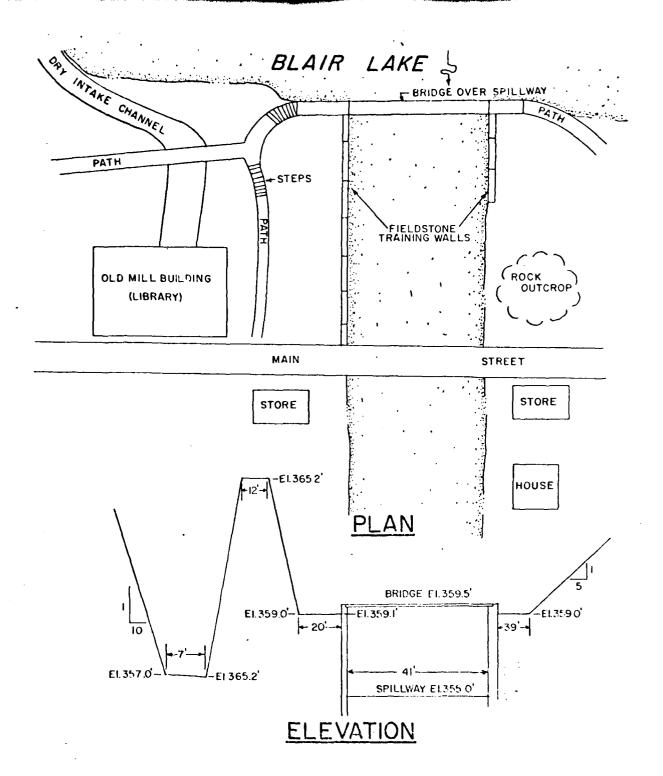
- b. Alternatives. None recommended.
- c. Operating and Maintenance Procedures

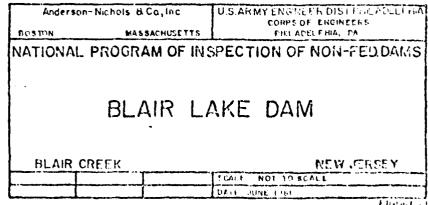
The owner should accomplish the following items soon:

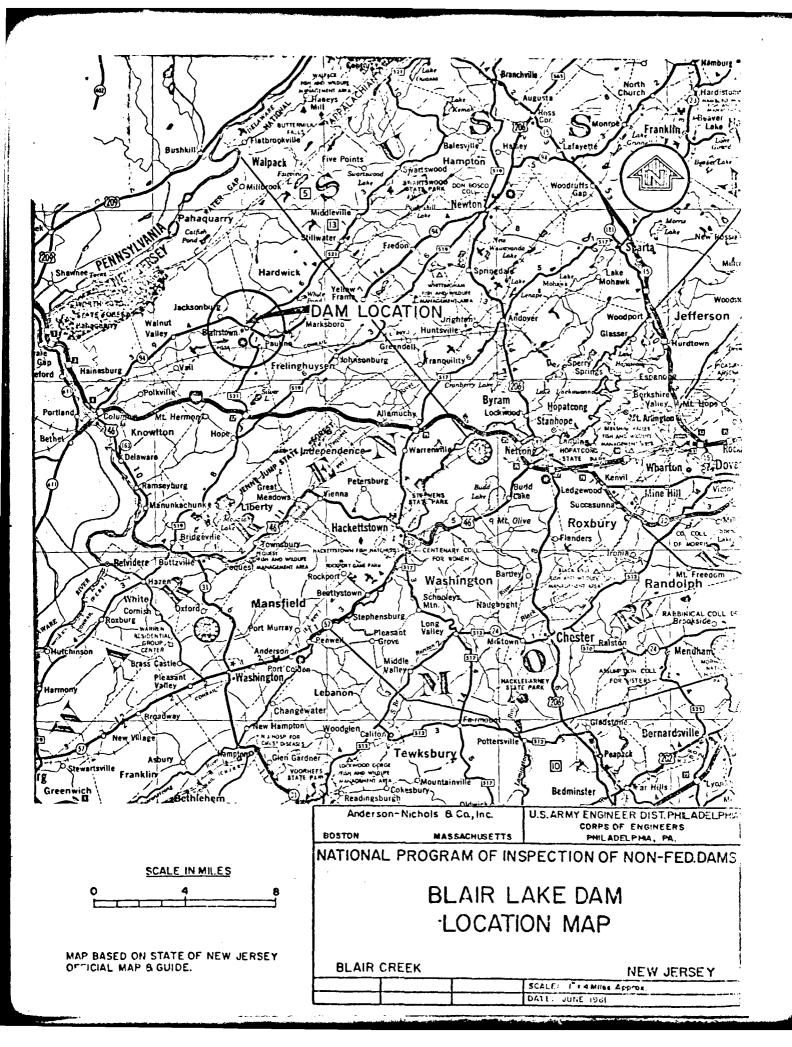
Develop an emergency action plan which outlines actions taken by the owner to minimize downstream effects of an emergency at the dam.

The owner should do the following in the near future:

Develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam.







APPENDIX 1

CHECK LIST

VISUAL INSPECTION

BLAIR LAKE DAM

Check List Visual Inspection Phase 1

| Coordinators            | 1 1                         | Inspection 342' NGVD                                   |
|-------------------------|-----------------------------|--|
| State NJ00774           | 450<br>Temperature 650      | stion 355.2' NGVD Tailwater at Time of Inspection 342' |
| County Warren           | Fair, mild<br>Weather Clear | spection 355.2' NGVD                                   |
| Name Dam Blair Lake Dam | Date(s) Inspection 4-27-81  | Pool Elevation at Time of Inspect                      |

Inspection Personnel:

| F.D.Deane | K. Stuart |            |  |
|-----------|-----------|------------|--|
| W. Guinan | S. Gilman | R. Murdock |  |

R. Murdock/F.D.Deane Recorder

Mr. J. Ernest Rea, Treasurer of Blairstown Academy, dam owners, accompanied the inspection team.

# CONCRETE/MASONRY DAMS

| VISUAL EXAMINATION OF                            | OBSERVATIONS   | REMARKS OR RECOMMENDATIONS                                      |
|--|--|---|
| SETEPAGE OR LEAKAGE                              | Water flowing over spillway - unable to inspect for seepage.   | Inspect during no flow condition over spillway.                 |
| STRUCTURE TO<br>ABUTHENT/EMBANKMENT<br>JUNCTIONS | Some rock blocks have been displaced on right abutment in vicinity of downstream face of dam. Erosion adjacent to toe of dam on left side. | Restore and/or replace<br>blocks of rock and<br>repair erosion. |
| DRAINS   | Not visible  |   |
| WATER PASSAGES                                   | Not visible  |   |
|  |  |   |

Appears to be bedrock on right side of dam. Not visible on left side of dam.

FOUNDATION .

# UNGATED SPILLWAY

| VISUAL EXAMINATION OF             | OBSERVATIONS  | REMARKS OR RECOMMENDATIONS                        |
|-----------------------------------|---|---|
| STONE MASONRY WEIR                | Numerous horizontal cracks noted in top walkway. Concrete cap visible on both sides of bridge, but not visible on central section. 4 ft. wide mortared cut stone cap; covered with algae, but appears to be in good condition. No indication of vertical or horizontal movement. Small amount of mortar missing on d/s joints. Some seepage is apparent on both sides near top of weir. |   |
| APPROACH CHANNEL                  | Clear and unobstructed.   |   |
| 1-3                               |   | •   |
| DISCHARGE CHANNEL                 | Clear wide and unobstructed. Bound by dry cut stone walls approx. 5 ft. 7 ft. high which train steam to bridge approx. 90 yards d/s. (Main Street of Blairstown). D/s training walls missing on both sides for approx. 15 ft. d/s of dam.   |   |
| BRIUGE AND PIERS<br>OVER SPILLWAY | Bridge is set on mortared cut stone spill-way abutments, no piers. It is constructed of steel channels bolted together w/channel  | Investigate impact of corrosion and make repairs. |

One section of railing

cross members & a wooden plank deck which is worn but solid. Railings also along approaches to bridge. Moderate weathered wood plank deck. Wrought iron gusset plates badly corroded.

| VISUAL EXAMINATION OF  | OBSERVATIONS  | REMARKS OR RECOMMENDATIONS |
|--|---------------|----------------------------|
| CRACKING AND SPALLING OF<br>CONCRETE SURFACES IN OUTLET<br>CONDUIT | NA            |                            |
| INTAKE STRUCTURE   | NA            |                            |
| OUTLET PIPE  | None observed |                            |
| OUTLET CHANNEL   | NA            |                            |
| EMERGENCY GATE   | None observed |                            |

# RESERVOIR

| VISCAL EXAMINATION OF | OBSERVATIONS   | REMARKS OR RECOMMENDATIONS |
|-----------------------|--|----------------------------|
| SIODES                | Gradual to moderately sloped,<br>some wooded areas, open grassed<br>area.                |                            |
| SEDIMENTATION         | Appears to be appreciable sedimentation below the reservoir surface in front of the dam. |                            |

# DOWNSTREAM CHANNEL

| VISUAL EXAMINATION OF                         | OBSERVATIONS   | REMARKS OR RECOMMENDATIONS          |
|---|--|-------------------------------------|
| CONDITION<br>(OBSTRUCTIONS, DEBRIS, ETC.)     | Clear, unobstructed, training walls, steep valley on left d/s bank and Library on right would confine flow.  | ing<br>t<br>ight                    |
| SLOPES  | Steep.   |                                     |
| APPROXIMATE NO.<br>OF HOMES AND<br>POPULATION | Up to 8 homes and businesses. Population affected 20 - high hazard. Blairstown business district affected by breach of dam. Flow would divert around railing of Main St. bridge and former mill (now Town Library) | igh<br>iss<br>th of<br>cound<br>and |
|   |  |                                     |
|   |  |                                     |

# DESIGN, CONSTRUCTION, OPERATION ENGINEERING DATA CHECK LIST

ITEM

REMARKS

PLAN OF DAM

None found

Prepared for this report. REGIONAL VICINITY MAP CONSTRUCTION HISTORY

Memoirs of Blair indicate the dam was built between 1902-03. Upstream side was sealed with 1,500 cubic yards of clay and earth along the spillway and the left embankment in 1960.

None found TYPICAL SECTIONS OF DAM

None found

HYDROLOGIC/HYDRAULIC DATA

OUTLETS - PLAN

- DETAILS

None found

- DISCHARGE RATINGS

- CONSTRAINTS

None found RAINFALL/RESERVOIR RECORDS

REMARKS None found DESIGN REPORTS ITEM

GEOLOGY REPORTS None for

None found

DESIGN COMPUTATIONS
HYDROLOGY & HYDRAULICS
DAM STABILITY None found
SEEPAGE STUDIES

1-8

MATERIALS INVESTIGATIONS
BORING RECORDS
LABORATORY
FIELD

POST-CONSTRUCTION SURVEYS OF DAM None found

BORROW SOURCES

Unknown

REMARKS None found MONITORING SYSTEMS :: E E

Memoirs of Blair see "CONSTRUCTION HISTORY" NODIFICATIONS

None found

HIGH POOL RECORDS

POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS

None found

PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION None found REPORTS

MAINTENANCE OPERATION RECORDS

None found

| REMARKS |  |
|---------|--|
| ITEMS   |  |

SPILLMAY PLAN

SECTIONS

DETAILS

None found

OPERATING EQUIPMENT PLANS & DETAILS

None found

## CHECK LIST HYDROLOGIC AND HYDRAULIC DATA ENGINEERING DATA

| DWITHMO | E AKEA CI | TARACTERISTICS: 10.      | os square miles, moderate slope, |
|---------|-----------|--------------------------|----------------------------------|
|         |           | · _ w                    | ooded                            |
| ELEVATI | ON TOP NO | ORMAL POOL (STORAGE      | CAPACITY): 355' NGVD (24 acre-   |
|         | ·         |                          | feet)                            |
| ELEVATI | ON TOP FI | LOOD CONTROL POOL (      | STORAGE CAPACITY) Not applicable |
| ELEVATI | ON MAXIM  | UM TEST FLOOD POOL:      | 370' NGVD                        |
| ELEVATI | ON TOP D  | \M:                      | 359.0' NGVD                      |
| SPILLWA | Y CREST:  | Uncontrolled             | masonry                          |
| a.      | Elevat:   | ion                      | 355' NGVD                        |
| b.      | Туре _    | ·                        | Broad crested                    |
| c.      | Width     | <del></del>              | 4 feet                           |
| đ.      | Length    |                          | 41 feet                          |
| е.      | Locatio   | on Spillover <u>Righ</u> | t center of dam                  |
|         |           | and Type of Gates        |                                  |
| OUTLET  | WORKS: _  |                          | None                             |
| HYDROME | TEOROLOG: | ICAL GAGES:              | None                             |
| MAXIMUM | 1 NON-DAM | AGING DISCHARGE:         | 984 cfs                          |

APPENDIX 2

PHOTOGRAPHS

BLAIR LAKE DAM



April 22, 1981

View looking at right upstream dam and spillway abutment; upsloping berm is left bank of old mill race. Note erosion and growth of large trees with roots exposed adjacent to dam.



February 18, 1981

View looking in downstream direction along axis of old mill race; roof of old mill building (now a public library) is just above arched bridge.



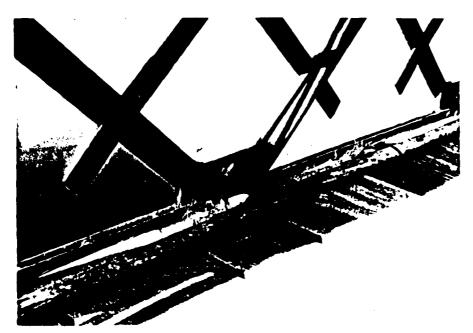
April 22, 1961

View of downstream left spillway abutment contact; note trees up to 14-inch diameter on slope, erosion, debris, and portions of lined downstream channel wall missing.



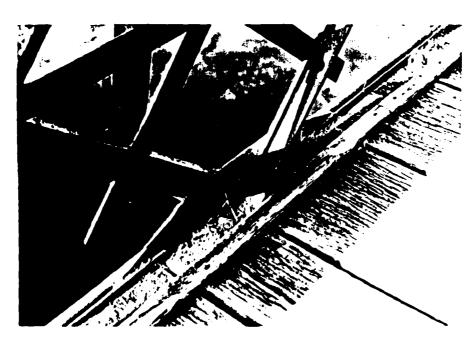
April 22, 1981

View of exposed bedrock contact at right spillway abutment.



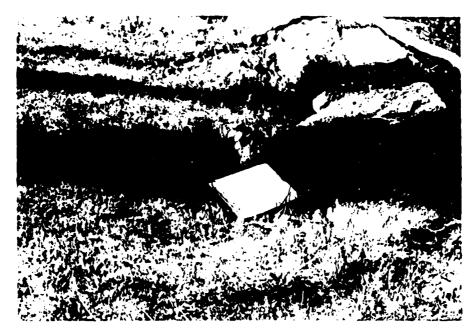
April 22, 195

Gusset plates rusted through on bridge over spillway.



April 22, 1981

Rust eaten gussets on upstream truss; note that rust is eating into truss angle bars.



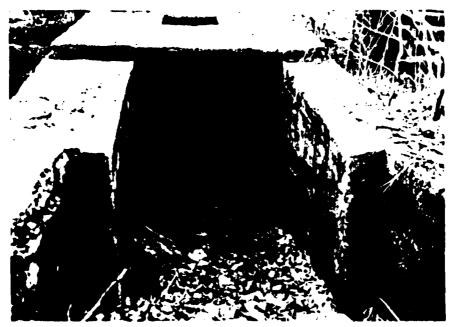
As it is

View of erosion to right downstream channel wall near sprinway; rule could be extended 2 feet into opening.



Etosion typical of many locations along lined downstream channel at top of bank.

April 27, 101



View of intake at head of old mill race at mill building on Main Street 200 feet downstream of dam.

February 18, 1981



April 22, 1981

View looking upstream across reservoir at inlet from Blair Creek; note that flow must turn nearly a right angle to pass over spillway.



April 22, 1981

View looking at downstream channel from right bank at dam; note Main Street Bridge.

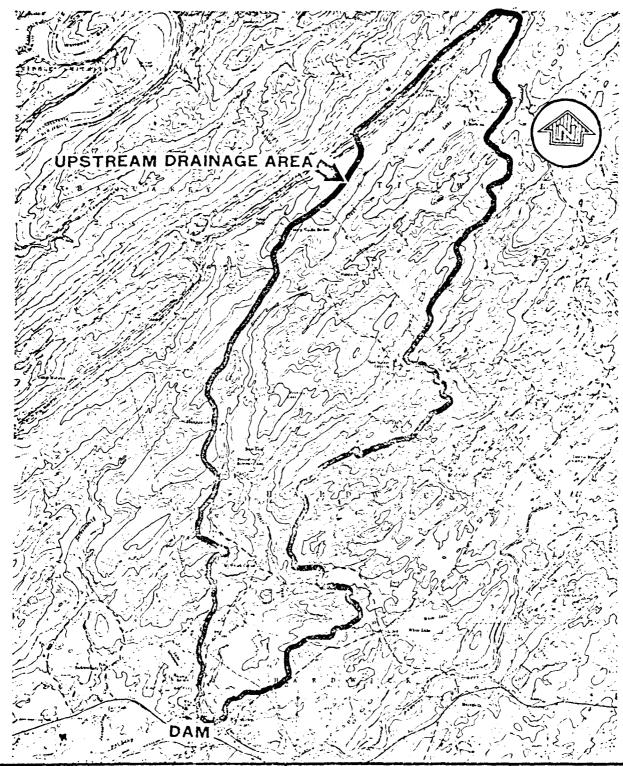


April 22, 1981

View looking downstream from downstream side of Main Street Bridge.

# APPENDIX 3 HYDROLOGIC COMPUTATIONS

BLAIR LAKE DAM



NATIONAL PROGRAM OF INSPECTION OF NON-FED. DAMS

BLAIR LAKE DAM
BLAIRSTOWN TOWNSHIP, NEW JERSEY

REGIONAL VICINITY MAP

**JUNE 1981** 

DEPARTMENT OF THE ARMY
PHILADELPHIA DISTRICT, CORPS OF ENGINEERS
PHILADELPHIA, FENNSYLVANIA

nderson-Nichols & Company, Inc. BOSTON, NA

SCALE IN MILES

0 1/2

MAP BASED ON U.S.G.S.7.5 MINUTE QUADRANGLE SHEETS. BLAIRSTOWN, N.J. 1954, REVISED 1971, AND FLATBROCKVILLE, N.J., PA. 1954, REVISED 1971.

Sheet No. / of /3

Date 4/19/81

Computed 7/4

Checked C.P.D

\* - Linear interpola

JOB NO.

11

14

17

19

32 33

34 35

2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 3

QUARES

#### INFLOW HYDROGRAPH

The inflow hydrograph for Blair Lake will be routed out flow

from Bass Lake + Local inflow downstream of Bass

Lake by SCS method.

Bass Lake has already bean run using these data:

12 DA = 5.959 mi.

13 Log = 3.3 hr.

precipe 22.2 inches

15 Use 11290, 12390, 13300, 1420% for 10to of 6,12,24, and ul-hourstorms to inis

16 Loss data: initial loss: 100 incom: loss rate of 0.15 m/hn

200 30-minute timesteps

18 Starting el = 100.1

| Storage |
|---------|
| 0       |
| 15,2    |
| 32.6    |
| 49.9 *  |
| 67,3 *  |
| 84.6    |
| 102 4   |
| 119     |
| 137 *   |
| 154     |
|         |

3 reaches from Bass Lake to Blair Lake.

Reach 1= 1630 feet Slope = 180 = 0.11

19

22

23

25 26

27 28

29 30

SQUARES 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 1/4 IN. SCALE

Typical cross section.

(15, 15) (15, 10) (50,5) (55:)

N= 0.05 channel 0.10 overbanks

(50,0) (65,0)

Reach 2 = 6,000 feet. Slope = 140 = 0,023

typical cross section:

1=0.05 channel =0.10 overbanks

Resol 3 = 10,000 Feet, Slope = 85 = 0.008

 $(0,15) \qquad (520,15) \qquad (520,15) \qquad (520,15) \qquad (250,5) \qquad (270,0)$ 

n: 0.05 channal =0.10 Overbanks

Localinflow to Blair Loise

Area: 5.0 mil Vse loss and storm characteristics same as Bass Lake

Sheet No. 3 of 13
Date 4/2://C
Computed Chacked

JOB NO.

QUARES

TIME of CONCENTRATION

1 Texas Highway Mathod

for woods, velocity = 3 fps.

Total Te = 3+ 1.67+2.22+0.38= 7,22 hrs.

23 2 Soil and Noter Conservation

XUARES 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 /4 IN. SCALE

```
@ Weston, or SCS T.R. #55
```

$$V = \frac{1.49}{0.05} (0.45)^{2/3} (0.02)^{\frac{1}{2}} = 2.5 fps$$

$$V = \frac{1.49}{0.05} (0.28)^{2/3} (0.013)^{\frac{1}{2}} = 4.24 ps$$

Wy Karby

Overland 
$$T_c = 0.83 \left( \frac{NL}{L^{57}} \right)^{0.467} N = 0.7, l = 3,600, s = 0.111$$

QUARES 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 33 /4 IN. SCALE

### Stage- Discharge Curve

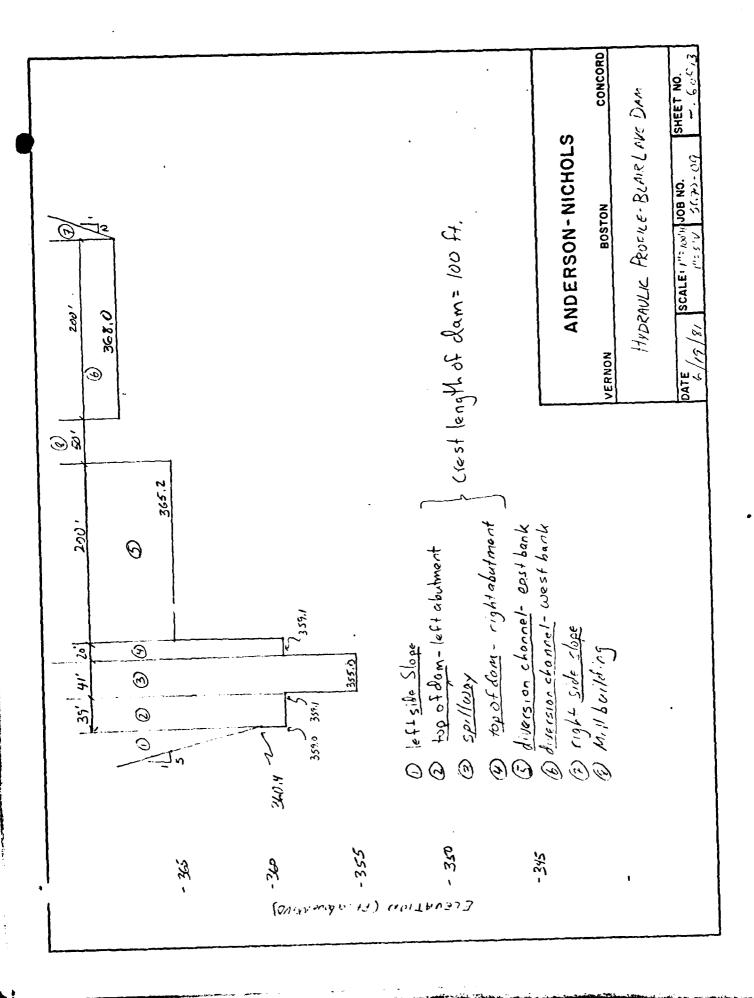
The hydraulic profile of Blair Dam is shown on page 6.

The diversion channel to the right of the spillway is blocked by a closed and appearently inoperable) gate at the mill building and high Channel bonks. If the water rises above 365.2, it will tear to flow over the east bank of the diversion Channel into Blair Creek downstream of the dam. This serves as an earth weir about 300 feet long. In plan view:

| N | 1 | high light bonk Chigher than

18
19
20
N
Channel
channel
channel
ground
ground
ground
ground
ground
ground

control extends as the black line, which is the line ilmunas the hydraulic profice



12

13 14 15

39

SQUARES 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 2

Stage Vs. Discharge

See profile on p 6. We will assume the spillway bridge has regligable offer discharge

Spillwoy: section (3) Q= 3.0 L3H3/2 = 3.0 (41) (E-365.0)3/2

Top of Dam: [sections 2 and 4) Q= 2.8 L2 H2312 + 2.8 L4 H4312 = 2.8 (39) (E-359.05) 312 + 2.8 (20) (E-359.1) Assume Aug. El. of section () = 359 1+359 = 359.05

Old Diversions channel: [sections of and O/Q= 2.61.5 Hg 3/2 + 2.6 Ly 1/6" = 2.6 (200) (E-365.2) 3/2 + 2.6 (700) (E-365

Side Sloses ( [Sections ] and D) 0= 2.6 L, H, 3/2 + 2.6 L, H, 3/2 = 2.6 (5(E-360.4))[(0.5) (E-360.4)] (0.5) (E-360.4) (0.5)

| _  |                  |                 |                   | 4          |           |           | <u> </u>    |         |
|----|------------------|-----------------|-------------------|------------|-----------|-----------|-------------|---------|
| 20 | ELEVATION        | DESCRIPATION    | HEAD Fraue        | a spillway | Otopostan | apir chan | Os de super | DOTAL   |
| 21 | (Ft, above NGVD) |                 | SPILLARY (RESILA) |            | ((FS)     | ((FS)     | ((12)       | (c = 5) |
| 22 |                  |                 |                   |            |           |           |             |         |
| 23 | 355              | spillway crest  | 0                 | 0          | 0         | 0         | 0           | 0       |
| 24 | 356              |                 | 1                 | 123        | 0         | 0         | 0           | 123     |
| 25 | 357              | _               | 2                 | 348        | 0         | 0         | 0           | 34.5    |
| 26 | 358              | -               | 3                 | 639        | 0         | 0         | 0           | 67      |
| 27 | 359              | top of for      | 4                 | 184        | 0         | 0         | 0           | 374     |
| 28 | 360              | -               | 5                 | 1,375      | 149       | 0         | U           | 1,524   |
| 29 | 361              | ~               | 6                 | 1,808      | 444       | 0         | 1           | 7,253   |
| 30 | <b>3</b> 63      | -               | 8                 | 2,783      | 1,289     | 0         | 50          | 4,122   |
| 31 | 365              | d'insistrations | 10                | 3,890      | 2,387     | 0         | 209         | 6,486   |
| 32 | 365,2            | west bonk       | /5, Z             | 4,007      | 2,509     | 0         | 232         | 6,748   |
| 33 | 366              | -               | //                | 4,417      | 3,016     | 372       | 341         | 8,216   |
| 34 | 368              | d version shows | 3                 | 5,765      | 4,411     | 2,437     | 732.        | 13,345  |
| 35 | 370              | -               | 15                | 7,146      | 5,772     | 6,939     | 1,364       | 21,421  |
| 36 |                  |                 |                   | , <i>'</i> |           |           | 1           | ĺ       |
| 37 |                  |                 |                   |            |           | 1         |             |         |
| 38 | I                | l               |                   |            |           |           |             |         |

|                | ב<br>ה   | 6/22/8   |             |  |                  | P. 9 of 1. | 3           |
|----------------|----------|----------|-------------|--|------------------|------------|-------------|
| E DAM          | 3        |          |             |  |                  |            |             |
| BLAIR LAVE DAM | <u>S</u> | 35       |             |  |                  |            |             |
| 8              | N .      |          |             |  |                  |            |             |
|                |          | <b>b</b> | CRP         |  |                  |            | \$ 000      |
|                |          |          |             |  |                  |            | :<br>:      |
|                |          |          |             |  |                  |            |             |
|                |          |          |             |  |                  |            | 2           |
|                |          |          |             | of the second  |                  |            | Discharge ( |
|                |          |          |             |  |                  |            | Q<br>2, 0   |
|                |          |          |             |  |                  |            |             |
|                |          |          |             |  |                  |            | 0,000       |
|                |          |          |             | 2000   | Toja             |            |             |
|                |          |          | رى در       | 3. 30.2<br>C. C. C. S. | 200              |            |             |
|                |          |          |             |  |                  | 8          |             |
|                | •        |          | G 5/1/ 3/10 | į  | 6)<br> 01/61/1/2 | )<br>      | # CO        |

Subject Blair Lake

JOB NO.

21

> 29 30

32

**3Q**UARES 1/4 IN, SCALE 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 3

Stage Vs. Storage

Area at pond surface = 4.3 acres (at 355'msl)

" " alev. 360 = 14.3

" eler. 380 = 31.6

" S45 Que.

Storage = 0 at 340.7, bottom of reservoir

Storage = 24 acre- feet at spillway crest

| 12<br>13 | Elevation<br>(Fr. skore 175 vs) | Surface Area<br>(Peres) | Average S.A.<br>(Pores) | · Incremental  STORAGE  (Acro-fo-t) | Storage<br>(Acra-feet) |
|----------|---------------------------------|-------------------------|-------------------------|-------------------------------------|------------------------|
| 14<br>15 | 3 <i>55</i>                     | 4.3                     |                         | İ                                   | 24                     |
| 16<br>17 | 360                             | 14.3                    | 9.3                     | 46.5                                | 70.5                   |
| 18<br>19 | 3%)                             | 31.6                    | 22.95                   | 459                                 | S 29.5                 |

Stage us. Storage plothed on p. 10

P. 10 0 5

13

TAGE 19 X 10 TO THE INCH 2 X 10 PLONES

Subject Starr Lake

Sheet No. // of 13
Date 6/22/07
Computed Checked Cir 9

JOB NO.

11

16 17

19

20 21

23 24

26

27 28 29

30

31 32 33

35 36 37

QUARES /4 IN. SCALE

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30

### Do wastream Amilysis

Downstream of Blair Lake Dam, Blair Creek runs 240 feet
through Blairstown to The Pauline Will. The creek is crossed by Illain
Street bridge about 300 feet below the bridge. There are I wo houses
and the Town Library at the bridge, about 8 feet above the stream invent
Downstream of Main Street, there are 3-4 houses about 6-8 feet

above the invert. Sketch: Blair Lake Dam 160 Diversion Charrel 1N Main ST. Eft above invert (t) 88+ above france (ft accomments - three 7 fl above in cert (4)

Packer Kill

39 40

38

Increase of Q.7 feet in 25 mortes would cause a significant increase to the Inzard of loss of life.

30

31

32 33 34

36 37

38 39 40 3. 1/2 PMF overtops the dam by 7.6 feet,

The spillway is seriously inadequate.

Subject Blair Lake Anderson-Nichols & Company, Inc. JOB NO. QUARES 18 19 20 21 22 23 24 25 26 27 28 29 /4 IN. SCALE Overtopping Analysis 2 -1.0 7 9 10 - 0.8 11 かえず 12 13 0.6 15 DERCENT 16 17 18 0.4 19 20 21 22 0.2 23 24 25 SPILLWAY CAPACITY, 984 cfs, ~ 500 FAF 26 5,000 27 15,000 70,000 12,000 28 Discharge (crs) 29 30 31 32 33 34 35 36 37

38 39 40 APPENDIX 4

HEC-1 OUTPUT

BLAIR LAKE DAM

|             | 10            |   |      |                  |  | REP  | 1094<br>1094<br>1094<br>1094  |                          |                              |                  |  |                          |                      |                                 |                |
|-------------|---------------|---|------|------------------|--|--|---|--------------------------|------------------------------|------------------|--|--------------------------|----------------------|---------------------------------|----------------|
|             | 6             |   |      | REPORT           |  |  | 137<br>108.1<br>6921<br>108.1   |                          |                              |                  |  |                          |                      | m                               |                |
|             | 1             | ANCI)<br>DANSHIP  |      | BASS LAKE        | 5.90 0 0 1 ND 112 173 133 142 3.3 0.15                               | ROUTE INFLOW HYDROGRAPH THROUGH BASS LAKE - INPUT FROM BASS LK | 1119<br>1019<br>1070<br>1070  | REACH 1                  | 115.                         |                  | 115.   |                          | 520.<br>15.          | BASS LAKE TO BLAIR LAKE         | 142            |
|             | .7            | REALE LAKE DAM GVERTOPPING AVALYSIS TOM GUICH ANCU-<br>NEW JERSITY DAM NO. 774 - WARKEN CHUNTY - MEAIRSTOAN TOWNSHIP<br>0.1.0.25.0.5.1.0 MULTIPLES OF PMF FROM 24-HOUR PMP<br>30.25.0.5.1.0.0 0.200 |      | EN FROM          | 133  | KE - INP   | 102.<br>3639.<br>105.1  | THROUGH                  | 90.                          |                  | 30.<br>10.   |                          | 395.<br>10.          | LAKE TO I                       | 133            |
|             | · 9 · · · · · | 7 - 10 A 3 - 400 A 3 - 400 A 3 - 400 A 3 - 400 B  |      | APUT TAK<br>IGNS | 173  | BASSLA   | 8<br>105<br>105<br>105<br>105<br>105<br>105<br>105<br>105<br>105<br>105 | FROM BASS LAKE           | 65.1                         | ~                | 65,1   |                          | 270 <u>.</u> 1       | - BASS                          | 123            |
| HEC-1 INPUT | 5.            | ANALYSI<br>CHUNT<br>PMF FED   | 0.1  | CAPH - 1         | 112  | THRUUGH  | 1001  |                          | 0.11                         | 1 REACH 2        | 0.023<br>65.<br>0.   | REACH :                  | 0.008<br>270.        | ROGRAPH                         | 112            |
| 1-234       |               | TOPP ING<br>PLESCE  | 0.25 | CRAPH C          | O Z  | ROGRAPH  | 49.9<br>103.1<br>103.1  | DROGRAFI                 | 1630.<br>50.                 | THROUGH          | •0009<br>•05<br>•0   | THROUGH                  | 10800.<br>250.<br>0. | FLOW HYD                        | Ë              |
|             | 3             | NU. 774   | 0.5  | SCS UNIT         |  | FLOW HYD   | 10001000100010001000100010000100001000010000                            | ROUTE OUTFLOW HYDROGRAFH | 49.9<br>5.9                  | RUUTE HYDROGRAPH |  | RDUTE HYDROGRAPH THROUGH | 249.9<br>5.9         | DEVELOP LOCAL INFLOW HYDROGRAPH |                |
|             | 2.            | LAKE DAY  | 1.0  | BASS LAP         | 0.00   | ROUTE IN   | 1015<br>1015<br>1016<br>1019<br>1019                                    | ROUTE OF                 | 8108<br>0.05<br>20.05<br>10. | RUUTE HY         | 20<br>10<br>20<br>20<br>20<br>30<br>30<br>30<br>30<br>30<br>30<br>30<br>30<br>30<br>30<br>30<br>30<br>30 | RDUTE HY                 | 0.00<br>1255<br>1055 | DEVELOP                         | 15.            |
|             | .11           | 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2   | FLOM | A1<br>12F1       | 0000<br>0000<br>0000<br>0000<br>0000<br>0000<br>0000<br>0000<br>0000 | A2   | 100.<br>100.<br>100.  | <b>A</b>                 | 0 1                          | 4                | 50.1   | 4.                       | 0 e                  | 97                              | 22.5.          |
|             | 10.           | 000-0   | iz.  | **;              | 54m272   | ¥;   | รูลเกเกเก<br>อุณ>mam  | *3                       | KWWKW<br>JNOX>               | ж,               | rarar<br>Snox>   | *;                       | YWWWX<br>YWUXX       | ¥.                              | SEATS<br>STEDO |

| 07                                      |   | 21421.<br>235.<br>335.  |
|---|---|---|
| .6                                      |   | 13345<br>1365<br>368  |
| 88                                      | LAKE  | 9674<br>1674<br>9674<br>9674<br>9674<br>9674<br>9674<br>9674<br>9674<br>9   |
| 7                                       | TO 3LA 11   | 1 AKE<br>4 122<br>353<br>1059<br>363  |
| 9                                       | . INFLOW  | 2253<br>363<br>361<br>361   |
| • | FT TUTAL  | 14800GH<br>984 -<br>359 -<br>359 -  |
| • | CUMBINE HYDROCKAPHS TO GET TOTAL INFLOH TO BLAIR LAKF | ROUTE INFLOW HYDROGRAPH THROUGH BY STOR 24. 348. 354. 355. 355. 357. 359. 355. 355. 357. 359. 41. 5. 59. 1.5  |
| 3                                       | HYDROCKA  | 17 L DW H YE<br>1374 + 1374 + 1374 + 1376 + 137 |
| D18894567899                            | COMB INE  | 8001E<br>STUR<br>3550<br>3550<br>3550<br>5910   |
|   | 47  | 84 0 0 1 1 3 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0  |
| 10.                                     | ችቪ<br>ችር  | XXNNNNNN<br>XNQM>MNFM   |
| LIE                                     | 64  | *<br><b> </b>   |

FLCOD HYDFOGRAPH PACKAGE (HTC-1) FEBRUARY 1981 AUR CATEUB/12/81 \*\*\*\*\*

BLAIR LAKE DAM NOVERTOPPING ANALYSIS TOM GOOCH ANCONEW JERSEY DAM NO. 774 - WARREN COUNTY - BLAIRSTOWN TOWNSHIP 0.1,0.25,0.5,1.0 MULTIPLES OF PMF FROM 24-HOUR PMP

2

\_

MINUTES IN COMPUTATION INTERVAL STARTING DATE STARTING TIME NUMBER OF HYDROGRAPH ORDINATES ENLING DATE ENLING TIME PAINT CONTRIL PLOT CONTROL HYCKIGGRAPH PLOT SCALE PYINT DIACNOSTIC MESSAGES OUTPUT CONTROL VARIABLES

DRAWT

USCAL

OSCAL

OSCAC

OSCA НУВРОСКАРН ТІМЕ ВАТА 30 164TE 1 0000 

COMPUTATION INTERVAL NCOA 10

SOUARE NILES FLET CUALC FEET PER SECOND ACKES FEET OCCREES FAHRENHEIT 99.50 HOURS DOM INDEPTH DRECIPITATION DEPTH PRECIPITATION DEPTH FERGIN, ELEVATION FICH STOKAGE VOLUME SURFACE AME TEMPFAATUKE

NUMBER OF PLANS MULTI-PLAN OPTION

> ڄ 3

0.25 MULTI-FATID DPTION KATIDS OF RUNDEF 1.CC 0.50

وجو ندر مده وده ودر بدر ودر بدر ودو باد ودو باد ودو باده وده ودو باده ودو باده ودو ودو ودو ودو ودو ودو ودو ودو

BASS LAKE INFLOW HYDROGRAPH - INPUT TAKEN FROM BASS LAKE REPORT INFLOW FROM SCS UNIT GRAPH COMPUTATIONS ¥

PRINT CONTROL PLOT CONTROL HYDROGRAPH PLOT SCALE OUTPUT COMIROL VARIABLES
JPRMI
JPRMI
O
CSCAL

9 4.0

SUINAASIY CHARACTERISTICS TAGEA TAGEA SUBBASIN FUNDER DATA 10 54

11 CF

BASE FLOW CHARACTERISTICS STEIN TIESD BELIN RASE FLOW RECESSION KTICK INDUCED RECESSION CONSTANT

\*

|  |   |                   | 619.<br>60.   |  |               |  |                              |   |                 |
|--|---|-------------------|---|--|---------------|--|------------------------------|---|-----------------|
|  |   |                   | 709.<br>77.<br>8.                                       |  |               |  |                              |   |                 |
|  |   |                   | 782.<br>96.<br>10.                                      |  |               |  |                              |   |                 |
| N TIME   |   |                   | GRAPH<br>D ORDINATES<br>1802.<br>119.                   | 99.50-HR<br>792.<br>20.696<br>6512.  | **<br>**      | 99.50-HR<br>792.<br>20.696<br>6512.  | ¢<br>•                       | 99.50-HK<br>396.<br>10.348<br>3256.   | *               |
| ACEX PRECIPITATION RANSPUSITION COEFFICIENT RANSPUSITION AKEA RANSPUSITION AKEA RANSPUSITION AKEA RANSPUSITION AKEA RANSPUSITION GISTON | INITIAL LOSS RATE<br>UNIFORM LOSS RATE<br>PERCENT IMPERVIOUS AREA |                   | UNIT HYDROGG<br>474. 5662.<br>236. 192. 153.<br>24. 19. | MAXIMUM AVERAGE FLUH<br>24-HR<br>3211.<br>20.242 20.611<br>6359.<br>5.90 SO MI | -             |  |                              | NAXIMUM AVERAGE FLOM<br>24-HR<br>1606.<br>1012.<br>1013.<br>3195.<br>5.90 SQ MI | ***             |
| A 200<br>200<br>200<br>200<br>200<br>200<br>200<br>200<br>200<br>200   | 100<br>010<br>010   | UNITCRAF          | 278.<br>30.   | 925018<br>14.577<br>45577<br>AREA  | \$ 1 5 H      | 11.000 11 | ess<br>H AT STR<br>N 1. KAT  | 6-H4<br>4625•<br>7•289<br>2293•<br>AREA =                                       | ф<br>ф          |
| PRICIPITATION DATE PRICIPITATION OAT PRICIPITATI | UNIFORM LOSS RATE<br>STATE<br>CNSTE<br>KTIMP                      | SCS DIMENSIONLESS | 1330<br>9776<br>387.                                    | (INCHES) (INCHES) COMULATIVE   | •             | (CFS)<br>(INCHES)<br>(AC-FTS)<br>CUMULATIVE  | OCC<br>HYDKJGRAPI<br>FDR PLA | (INCHES)<br>(AC-FT)<br>CUMULATIVE   | 0 0 0           |
| a a a  | 5   | S                 | 424<br>VBQ4   | 11 K<br>(HR)<br>43.00  |               | 11ME<br>(HR)<br>3.00   |                              | # (HI)  |                 |
| 12<br>FR   | 13 רח   | 14 00             |   | FEAK FLOW<br>(CFS)<br>12006.   | <b>•</b><br>• | FEAK F104<br>12600.  | Ф<br>Ф<br>Ф                  | FEAN FLOW<br>(CFS)<br>. 6006.   | <b>\$</b> \$ \$ |

|                           |   | . •   | 154.0<br>109.10<br>8777.                           |         |
|---------------------------|---|---|--|---------|
|                           |   |   | 137.0<br>108.10<br>6921.<br>108.10                 | 8777.00 |
|                           |   |   | 119.0<br>107.10<br>5137.<br>107.10                 | 6921.00 |
|                           |   |   | 102.0<br>106.10<br>3639.<br>119.00                 | 5137.00 |
|                           |   |   | 84.6<br>105.10<br>2422.<br>105.10                  | 3639.00 |
| *                         | 9.50-HR<br>198.<br>5.174<br>1628.               | 99.50-HP<br>79.070<br>7.070<br>651.                           | - 1NP<br>- 1NP<br>67.3<br>4.10<br>511.             | 2422.00 |
|                           | 72-10W<br>72-72<br>5-153<br>1621.               | 7 FL GW<br>7 109 5<br>2 109 5<br>6 4 9 5                      | * SS   | 1511.00 |
| ***                       | IVERAGE   | sas<br>11<br>1VERAGE  | 11 S 11 S S S S S S S S S S S S S S S S            | 796.00  |
| ,<br>z                    | MAXIMUM<br>24-14<br>24-14<br>25-06-1<br>15-92-1 | 18 0.10<br>HAX180<br>232<br>2.30<br>5.90 S                    | 15.2 101.10  | 355.00  |
| SPH AT STATIO             | 2   | # \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$    | 0 Z 0  | 65.00   |
| 444<br>HY <u>orograph</u> | COMULATIVE                                      | HYDRDGRAPH<br>HYDRDGRAPH<br>(INCHES)<br>(ACHES)<br>CUMULATIVE | A S S S S S S S S S S S S S S S S S S S            | 0.0     |
|                           | 4<br>111<br>121<br>100<br>100                   |   | **************************************             | CUTFLOW |
| 6                         | FERN FICH<br>(CFS)<br>3566.                     | FE FE OF 4 4 12 CO 2 1 CO 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | 15 NK<br>16 KG<br>17 RS<br>19 SE<br>20 SE<br>21 SE |         |

| oce WARNING &C                  | ٥                      | MODIFIED PULS KOUTING WILL BE<br>USE SHUKTER TIME INTERVAL OR | INC WILL                                | NUMERICALLY UNSTABLE  | FOR OUTFLOWS BETWEEN                     | 1511. 10 |
|---------------------------------|------------------------|---|---|---|--|----------|
|                                 |                        | <b>3</b><br>3<br>4  | _                                       | ****  | ***                                      | ,        |
|                                 |                        | HYDROGRAPH<br>FUR PLAN  | A T<br>1.                               | STATION AZ<br>RATIU = 1.00                                      |  |          |
|                                 | 11HE<br>(HR)           | (INCHES)  | 6-HR<br>9224.<br>14.536                 | MAXIMUR AVERAGE FLUH<br>24-HR<br>23-05.<br>23-05.<br>63-62.     | 99.50-HR<br>70-10-687<br>20.687<br>7509. |          |
|                                 | 11 ME<br>(HK)          |   | 6-HR<br>158.                            | NAXIMUY AVERAGE STORAGE<br>24-HR<br>72-HR<br>30.                | 99.50-HR<br>23.                          |          |
|                                 | 43.00<br>63.00         |   | 6-HR<br>109.33                          | MAXIMUM AVERAGE STAGE 24-HR 104.70 101.92                       | 99.50-HR<br>101.47                       |          |
|                                 |                        | CUMULATIVE  | E AREA =                                | 5.90 SQ MI  |  |          |
|                                 |                        | 0 4 3   | **************************************  | ***   | ***                                      |          |
|                                 |                        | HYDRUGKAPH<br>FOR PLAN  | PH AT STATIC                            | 11GN A2   |  |          |
|                                 | 11ME<br>(HR)<br>43.00  | (INCHES)<br>(AC-FT)   | 6-HR<br>4613•<br>7-270<br>2267•         | MAXIMUM AVERAGE FLOW<br>24-HR<br>1662-<br>10,097<br>3177-       | 99.50-HR<br>396.<br>10.353               |          |
| PEAK STCKAGE<br>(AC-FT)<br>128. | 117E<br>(HK)<br>63.00  |   | 6-HR<br>112.                            | MAXIMUM AVERAGE STORAGE   | 99.50-HR<br>16.                          |          |
|                                 | 11ME<br>(HP)           |   | 6-HR<br>106.73                          | MAXIMUM AVERAGE STAGE<br>24-HR<br>103.40 101.38                 | 99.50-HR<br>101.05                       |          |
|                                 |                        | CUMULATIVE  | E AREA =                                | 5.90 SQ 4I  |  |          |
|                                 |                        | ***   | 8                                       | ***   | ***                                      |          |
|                                 |                        | HYDEDGRAPH<br>FOR PLAN  | 4T ST4                                  | 116N 0.25 . A2  |  |          |
|                                 | 11PE<br>(15R)<br>43.00 | (CHESS)   | 6 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | MAXIMUM AVERAGE FLOW<br>24-HR<br>800.<br>573.<br>5.04.<br>1556. | 99.50-HR<br>198.<br>5.177                |          |
|                                 | 11x<br>03.00           |   | 6-HR<br>51.                             | MAXIMUM AVERAGE STORAGE   | 99.50-HR<br>11.                          |          |
|                                 | 11ME<br>(HP.)          |   | 6-HR<br>104-91                          | MAXIMUM AVERAGE STAGE<br>29-18<br>102.49                        | 99.50-HR<br>100.76                       |          |
|                                 |                        |   |   |   |  |          |

14 55 06.5

CUMULATIVE AKEA =

8777.

|     |   |  |                         | •   | 5.90 S0 M1        |
|-----|---|--|-------------------------|---|-------------------|
| *** |   | 99.50-HR<br>79.<br>7.071<br>652.                             | 99.50-HR                | 99,50-HR<br>100,50                              |                   |
| **  | IGN A2  | MAXIMUM AVERAGE FLUN<br>24-HR<br>2-103<br>2-013<br>633- 649. | MAXIMUM AVERAGE STORAGE | MAXIMUM AVERAGE STAGE<br>24-18<br>101.62 100.65 | 5.90 S0 MI        |
| *** | HYDRUGRAPH AT STATION<br>FOR PLAN 1. RATIO = 0.10 | (CFS) 915.<br>(INCHES) 1.4442<br>(AC-FT) 454.                | 6-HR<br>52.             | 103.22  | CUMULATIVE AREA = |
| *   |   | PEKK FLOW TIME (CFS) (MK) 11%5. 43.50                        | FEAK SICKAGE TIME (AR)  | FEET STAGE TIME (HR) 103.64 43.50               |                   |

| 22 KK          | 00000000000000000000000000000000000000  | ROUTE DJ  | ROUTE DJTFLOW HYDROGRAPH FROM BASS LAKE THROUGH REACH  | JGRAPH F                                | ROM BASS                                 | LAKE 1               | нкоисн   | REACH | <b>-</b> -                   |       |
|----------------|---|---|--|---|--|----------------------|----------|-------|------------------------------|-------|
| 23 KD          | OUTPUT CGHTR<br>IFRAT<br>IFLOT<br>GSCAL   | OUTPUT CONTROL VARIABLES JERGT 0 PLUT CONTROL JERGT 0., HYCROGRAPH PLOT SCALE | PRINT CONT<br>PLUT CONTE<br>HYCRUGRAPH   | rrol<br>Ob<br>Forns                     | CALE                                     |                      |          |       |                              |       |
|                | HYDROGRAPH ROUTING DATA   | TING DATA   |  |   |  |                      |          |       |                              |       |
| 24 RS          | STORAGE ROUTING HSTPS ITYP RSVRIC   |   | STOK TYPE OF INITIAL CONDITION 1.00 INITIAL CONDITION 0.0 INITIAL COMPITION 0.0 MORKING R AND D COFFICIENT | SUBREAC<br>VITIAL<br>SAUTTION           | HES<br>ONDITION<br>FFFICIENT             | _                    |          |       |                              |       |
| 25 RC          | NORWAL DEPTH CHANNEL KOUTING  ANCH 0.100 LEIT OVERDANK N-VALUE ANCH 0.050 HIGH OVERDANK N-VALUE PLATH 1630. RIGHT ENGTH SEL 0.1100 RIGHT BLUE ELMAX CALEVOR | CHANNA<br>0000<br>0000<br>0000<br>0000<br>0000<br>0000<br>0000                | TING<br>TEFT OVER<br>MAIN CHAY<br>REACH OVER<br>REACH EVE<br>EVER SEL                                      | A K K K K K K K K K K K K K K K K K K K | <i>alue</i><br>Luf<br>Value<br>Orage/out | ונונאנ               | :ALCULAI | NOIL  |                              |       |
| 27 KY<br>25 KX | ELEVATION<br>01STANCE   | 15.00 10.00 25.00 49.90 50.00 65.00 65.10 90.00 10.00 10.00                   | 64 K == 5<br>60 5 = 5<br>60 5 = 5<br>60 5 6 5  | CT 10N DA                               | 74 MAIN CHA!                             | 1NFL<br>000<br>65.00 | 9        | 000   | 16HT QVERE<br>10.00<br>90.00 | . A ≥ |

| 27.12                                 | 2920.77               | 15:30        |                                  |     |                        |  |                                |                                |              |                | •                         |                                     |                                  |                              |            |          |
|---------------------------------------|-----------------------|--------------|----------------------------------|-----|------------------------|--|--------------------------------|--------------------------------|--------------|----------------|---------------------------|-------------------------------------|----------------------------------|------------------------------|------------|----------|
| 3.90                                  | 2338.21<br>14658.39 1 | 14:21        | 16905.                           |     |                        |  |                                |                                |              |                |                           |                                     |                                  |                              |            |          |
| 3.18                                  | 1846.67               | 13.42        | 0. 10                            |     |                        |  |                                | •                              |              |                |                           |                                     |                                  |                              |            |          |
| 19.02                                 | 10808:17              | 12:63        | BETWEEN                          |     |                        |  |                                |                                |              |                |                           |                                     |                                  |                              |            |          |
| LOW CURVE<br>2.23<br>15.44            | 1112.24               | 3.95         | OUTFLOWS 8                       | *** |                        | 99.50-HR<br>792.<br>20.687<br>6509.        | 99.50-HR                       | 99.50-HR<br>1.49               |              | *              |                           | 99.50-HR<br>396.<br>10.353<br>3258. | 99.50-HR<br>1.                   | 99.50-HR<br>1.02             |            | **       |
| AGE -001F<br>1.76<br>13.10            | 7744.44               | 3.16         | F.0.2                            | *   |                        |  | 510R4GE 9                      | STAGE 9                        | . •          | *              |                           |                                     | STORAGE 9                        | 72-HR 9                      |            | *        |
| CCMPUTED STORAGE - OUIFLOW 1.33 13.10 | 522.29<br>6479.98     | 10.26        | CALLY UNSTABLE REACH LENGTH      | •   | 43                     | AVERAGE FLUM<br>72-HR<br>1090:<br>9 20:611 | MUN AVERAGE STO<br>24-HR<br>6. | VERAGE                         | ¥ ¥          | *              | 43                        | AVERAGE FLOW<br>545-HR<br>7 10-311  | XIMUM AVERAGE STO<br>24-HR<br>3. | VERAGE                       | IW         | *        |
| 0.89<br>9.13                          | 580.42                | 1.58         | OR LUMGER RE                     |     | STATION 1.00           | MAXIMUM 24-HR 32056<br>20-219<br>5352.     | MAXIMUM<br>24-HI               | MAXIMUN A<br>24-118<br>5-55    | 5.90 56      |                | 11 UN 0.50                | MAXIMUM 24-HR 1602-1602-173         | MAXIRUM 24-HS                    | MAXIMUM 1<br>24-18<br>3.69   | 5.90 50    |          |
| 20°<br>44<br>43                       | 93.69                 | 0.79<br>8.68 | G 41LL                           | *** | 14<br>1.               | 6-HR<br>9258:<br>14.542<br>4576.           | 6-HR<br>15.                    | 6-HR<br>11.74                  | E AKEA =     | **             | AH AT STATION AN I. RATIO | 6-HR<br>4615-<br>7-872<br>2288-     | 6-84<br>8                        | 6-HR<br>8.74                 | E AREA =   | ***      |
| 0.0                                   | 3611.68               | 9.6          | MARNING #50 MCOIFIED PULS KOUTIN | 444 | HYDKOGRAPH<br>FOR PLAN | (INCERT)                                   |                                |                                | CUMULATIVE A | \$ 2 <b>\$</b> | HYDROGRAPH<br>FOR PLAN    | (INCHES)                            |                                  |                              | CUMULATIVE | 0 4 4    |
| STURAGE                               | OUTFLOW               | ELEVATION    | PAGOIF<br>USE S                  |     |                        | 4 3.00<br>4 3.00                           | 11KE<br>(HR)<br>43.00          | 11HE (HR)                      |              |                |                           | A STAN                              | TIME (HR)                        | 4<br>(HR)<br>00.00           |            | •        |
| VI                                    | J                     | 313          | ete nirring a                    | *** |                        | FEAK FLGW<br>(CFS)<br>11966.               | FEAK STERAGE<br>(AC-FT)        | FEAR. STAGE<br>(FLET)<br>15-14 |              | ***            |                           | FEAK FLOW (CES) 5589.               | FEAK STORAGE<br>(AC-FT)          | PEAK STAGE<br>(FCET)<br>9.91 |            | <b>Q</b> |

|             | •                        |  |                          |   |            |  |                        |   | ·                       |  |            |                         |  |  |                      |   |  |
|-------------|--------------------------|--|--------------------------|---|------------|--|------------------------|---|-------------------------|--|------------|-------------------------|--|--|----------------------|---|--|
| 444         | •                        | 99.50-HR<br>198.<br>5.17<br>1629.                  | 99.50-HR<br>0.           | 99.50-HK<br>0.57                            |            | ***                                    |                        | 99.50-HR<br>2.071<br>652.                             | 99.50-HR<br>3.          | 99.50-HR<br>0.36                             |            | *** *** *** *** *** *** |  |  |                      |   | -VALUE<br>N-VALUE<br>N-VALUE<br>STGRAGE/COTFICH CALCULATION  |
| 200         | ICN A3                   | MAXIMUN AVERAGE FLOM 24-11R ANO. 5-062 5-062 1556. | MAXIMUM AVERAGE STORAGE. | MAXIMUM AVERAGE STAGE<br>24-HR<br>2.61 0.92 | 5.90 SO MI | ***                                    | TICN A3                | MAXIMUM AVERAGE FLOH .<br>219.<br>2-013 2-063<br>633. | MAXIMUY AVERAGE STORAGE | MAXIMUM AVERAGE STAGE<br>24-HR 72-HR<br>1-41 | 5.90 SG MI | *** *** *** *** ***     | OGRAPH THROUGH REACH 2                               | PRINT CONTROL<br>PLOT CONTROL<br>HYDROGRAPH PLOT SCALE : |                      | NUMBER OF SUBREACHES TYPE OF INITIAL CANDITION INITIAL COMBITION WORNING R AND U COFFICIENT | DUTING<br>LEFT OVERSANK N-VALUE<br>OF MATH CHANNEL N-VALUE<br>NO FEACH LENGTH<br>NO FYERSY SLUPE<br>OF MAX. ELEV. FOR STORAGE/COUT |
| 0<br>0<br>4 | AT STATION<br>1. RATIO * | 230°H<br>33°55°<br>1143°                           | 6<br>5.4<br>4.           | 6-HR<br>6.17                                | AREA =     | ************************************** | AT STA                 | 1 91 5 K  | 6-HR<br>2.              | 90<br>H-9<br>J-7                             | AREA =     | *                       | ROUTE HYDROG   | VARIABLES<br>3 P<br>0 P<br>0 P                           | ATA                  | 1 ST CO   | CHANNEL X00.1000.0000.0000.0000.0000.0000.0000.  |
| coo         | HYDKOGKAPH<br>FOR PLAN   | (17CHES)<br>(ACHES)                                |                          |   | CUMULATIVE | <b>9</b>                               | HYDROGRAPH<br>FOR PLAN | (INCHES)  |                         |  | CUMULATIVE | *** *** *** ***         | \$ \$ \$ \$ \$ \$ \$ \$                              | UT CONTROL<br>IPRNT<br>IPLOT<br>CSCAL                    | HYDROGRAPH ROUTING D | REVEIC  | NDRWAL DEPTH CHANN<br>ANCH<br>ANCH<br>FLNTH<br>FLNTH<br>ELVAX  |
|             |                          | 11ME<br>43.00                                      | 5E T18E (HE)             | •   |            |  |                        | EGS<br>ET +   | 6E 11 (HR)              | E TYME (HR)                                  |            | ***                     | 6 0<br>6 0<br>6 9<br>6 9<br>6 9<br>6 9<br>6 9<br>6 9 | OO.  | HYDR                 | ST.   | Q  |
| 900         |                          | FEAK FLUH<br>(CFS)<br>2584.                        | FLAK STGRAGE<br>(AC-FT)  | FEAN STACE (FIET)                           |            | 9 4                                    |                        | 40 H H H H H H H H H H H H H H H H H H H              | PESK STERAGE            | FEAK STAGE (FEET)                            |            | ****                    | 26 KK  | 29 10  |                      | 30 KS   | 31 KC  |

| SECTION DATA  49.90  69.00  69.00  69.00  69.00  69.00  7 40.42  8 238.83  8 238.83  8 238.83  8 238.83  8 238.83  8 238.83  8 238.83  8 238.83  8 238.83  8 238.83  8 238.83  8 238.83  8 20.83 | T DVERHANN SECTION DATA  T DVERHANN SECTION DATA  10.03  49.90  50.00  65.00  6 | T DVERNAR CROSS-SCCTION DATA  T DVERNAR CROSS-SCCTION DATA  T DVERNAR CROWNED  T D D D D D D D D D D D D D D D D D D   | T DVERTANK  T DVER | T DVERNACK STATE OF THE NOTE OF STATE O |
|--|--|--|--|--|
| T DVERHAUN =   | T DVERRAN SESSECTION DATA  T DVERRAN SESSECTION DATA  1,63   | T DVERIANY  T D D D D D D D D D D D D D D D D D D  | T DVERFANK  T DVER | TOVERLAND STATES TO THE MANY CHANNEL RIGHT UVERDANK RIGHT UND READER RIGHT UND READER  |
| CERDSS-SECTION DATA  ANN  ANN  ASSET 1100  245.90  26555  35.49  COMPUTED STORAGE -0UTP  245.90  245.90  245.90  245.90  245.90  245.90  ANIMUM AVERAGE FLOW  BAXIMUM AVERAGE STARGE  24.90  ANIMUM AVERAGE FLOW  BAXIMUM AVERAGE FLOW  COMPUTED STORAGE  45.20  ANIMUM AVERAGE STARGE  ANIMUM AVERAGE FLOW  BAXIMUM AVERAGE STARGE  COMPUTED STORAGE  ANIMUM AVERAGE STARGE  COMPUTED STORAGE  COMPUTED STORAGE  ANIMUM AVERAGE STARGE  COMPUTED STORAGE  COMPUTED STORAGE  ANIMUM AVERAGE STARGE  COMPUTED STORAGE  COMPUTED  | CCMDSS-SCCTION DATA  ANN CLANNEL  A95.90  65.00  65 | CCMDSS-SCCTION DATA  ANY CLANNELL  4 9.90  5.00  4 9.90  5.00  6.00  5.00  5.00  6.0 | CONTRINGED   CONTRICT   CONTRIC   | CCRDSS-SCCTION DATA  CCRDSS-SCCTION DATA  CCRDSS-SCCTION  CCRDSS-SCCTION  CCRDSS-SCCTION  CCRDSS-SCCTION  CCRDSS-SCCTION  CCRDSS-SCCTION  CCCRDSS-SCCTION  CCCRDSS-SCCTION  CCCRDSS-SCCTION  CCCCRDSS-SCCTION  CCCCRDS-SCCTION  CCCCRDSS-SCCTION  CCCCRDSS-SCCTION  CCCCRDSS-SCCTION  CCCCRDSS-SCCTION  CCCCRDS-SCCTION  CCCCCRDS-SCCTION  CCCCRDS-SCCTION  CCCCRDS-SCCTION  CCCCRDS-SCCTION  CCCCRDS-SCCTION  CCCCRDS-SCCTION  CCCCCRDS-SCCTION  CCCCCCRDS-SCCTION  CCCCCRDS-SCCTION  CCCCCCRDS-SCCTION  CCCCCCRDS-SCCTION  CCCCCCRDS-SCCTION  CCCCCCCCCCCCCTION  CCCCCCCCCCCCCCCTION  CCCCCCCCCCCCCCCCTION  CCCCCCCCCCCCCCCCCCCCTION  CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC   |
| DATALY CHANNEL  50.00  50.00  65.57  66.57  66.57  10.57  10.56  10.57   | DATA<br>MAIN CHANNEL   | DATA V CHANNEL 5.00 100 55.10 100 55.00        | DATA  WALLY CHANNEL  | DATAN CHANNEL 5.00 15.00 115.00 55.00 115.00 55.00 115.00 115.00 55.00 115.00 115.00 115.00 55.00 11        |
| 200 K AH CHO420 KHO TIAMA CI TI AH CHO CO KHO AH CHO CHO CHO CHO CHO CHO CHO CHO CHO CH  | CHANNEL  | CHANNEL  | CHANNEL FIGHT UVFRDANK  46.50  46.50  46.55  46.55  56.05  46.55  56.05         | CHANNEL  |
|  | 0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0<br>0.0   | 10.00 65.10 10.00.00.00.00.00.00.00.00.00.00.00.00.0   | 000 65.10 96.00 11.69 56.00 11.69 56.00 11.69 56.05.35 49.65.10 11.69 4199.24 496.219 5775.09 11.84 12.63 13.42 13.85 12.63 13.42 10.355 2.24  9.50-HR   |  |

|   |  | ~  |   |  |                   |  |  |  |  |   |                   |
|---|--|--|---|--|-------------------|--|--|--|--|---|-------------------|
| 7.9. 10-HK  | \$<br>\$<br>\$   | 99.50-HK<br>198.<br>5.176<br>1629.                       | 99.50-HR                                      | 99.50-HR<br>1.38                       |                   | **                                     |  | 99.50-HR<br>79.071<br>652.                                     | 99.50-HR   | 99.50-HR<br>0.62                            |                   |
| MAXIMUM AVI KAĞI STAÇI<br>24-11K<br>5-110<br>5-20 SG MI | ¢¢¢<br>HYDRGGRAPH AT STATIUN<br>FOR PLAN 1. RATIO = 0.25 | MAXIMUM AVERAGE FLOW<br>24-118<br>806.<br>5-051<br>1556. | MAXIMUM AVERAGE STORAGE<br>24-HR 72-HR<br>12. | MAXIMUM AVERAGE STAGE<br>24-HR<br>4-09 | 5.90 Su MI        | ***                                    | HYDROGRAPH AT STATION A4<br>FUR PLAN 1. RATIO = 0.10 | MAXIMUM AVERAGE FLOW<br>24-HR 72-HR<br>2-919 2-063<br>633-653- | MAXIMUM AVERAGE STORAGE<br>24-HR 72-HR 72-HR 75-HR 75-HR 75- | MAXIMUM AVERAGE STAGE 24-HR 24-HR 2-42 0-85 | 5.90 SQ MI        |
| 12.1<br>12.1<br>AKEA 116                                | A AT STATE   | 239-<br>2302-<br>11-623-<br>1423-                        | 6-HR<br>31.                                   | 6-HK<br>9.10                           | AREA =            | ************************************** | H AT STAT  | 600 • 4<br>1 4 4 7<br>2 4 4 4<br>3 • 6 •                       | 6-H2<br>13•  | 6-14<br>6-14<br>16-14                       | AREA =            |
| 6-HK<br>12-18<br>CUMULATIVE AKEA =                      | ###<br>HYDROGRAP<br>FOR PLA                              | (CFS)<br>(INCHES)<br>(AC-FT)                             |   |  | CUMULATIVE AREA = | <b>\$</b>                              | HYDROCRAP<br>FOR PLA                                 | (IVCHES)   | :  |   | CUMULATIVE AREA = |
| 111.<br>111.<br>100.                                    |  | 11HE<br>(HK)<br>43.50                                    | 11 K<br>(HK)<br>9.50                          | 1114<br>(HP)<br>43.50                  |                   |  |  | MAH W.   | 11vE<br>(PP)<br>63.50  | 1113<br>(HR)<br>69.50                       |                   |
| FE2K STACK<br>(75 E T)<br>(15.57)                       | 6 3 6  | FEAK FLOW (CFS)  | PEAK STURAGE<br>(AC-FT)                       | PEAN STAGE<br>(FLET)<br>10.28          |                   | 000                                    |  | FEAR FLUN<br>(CF.5)<br>1186.                                   | PEAK STERAGE<br>(AC-FT)<br>16.                               | PEAK STAGE<br>(FEET)                        |                   |

\*\*\* \*\*\* \*\*\* \*\*\* \*\*\* \*\*\* \*\*\* \*\*\* \*\*\*

| eso coc coc sea sec coc coc coc coc coc coc coc coc coc c |   |  |                         |   |   |
|---|---|--|-------------------------|---|---|
| #<br>#<br>#   |   |  |                         |   |   |
| #<br>#<br>#   |   |  |                         |   |   |
| <b>\$</b>   |   |  |                         |   | A T 101   |
| Ф<br>Ф  |   |  |                         |   | רכחר  |
| ∯<br>€:<br><b>⊕</b>                                       |   |  |                         |   | 7 CA  |
| \$<br>\$<br>\$  |   |  |                         | <b>-</b>  | TFLC  |
| *<br>*  | <b>6</b>                                |  |                         | STOR TYPE OF INITIAL CONDITION 1.60 INTIAL CONDITION 0.5 INTIAL CONDITION 0.5 WORKING R AND 0 COFFFICIENT | f<br>E 700  |
| ф<br>ф  | ROUTE HYDRJGRAPH THROUGH REACH 3        | CALE   |                         | HES<br>INDI   | ALUE<br>LUF<br>VALU<br>NRAG   |
| <b>*</b>  | ж<br>н                                  | . TO   |                         | 1 1000<br>1 1 1000  | X X X X X X X X X X X X X X X X X X X   |
| <b>\$</b>   | THROU                                   | TROL<br>FROL   |                         | SCA<br>AND<br>AND   | Arrivor.<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Frankori<br>Fra |
| \$<br>\$<br>\$  | грн 1                                   | T<br>CCC<br>FRANCE   |                         | #247<br>7047  |   |
| 0<br>8  | ROCK                                    | 98<br>47<br>14<br>14<br>15<br>15<br>15<br>15<br>15<br>15<br>15<br>15<br>15<br>15<br>15<br>15<br>15 |                         | 24.78<br>24.78<br>24.78   | STATE AND A STATE   |
| ζ<br>\$<br>\$   | нурь                                    | LES<br>000   |                         | ~~~~~~<br>~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~   | 20020 + 22  |
| ÷   | OU TE                                   | RIABI  | DATA                    | CLA   | 1000 · · · · · · · · · · · · · · · · · ·  |
| ë<br>6  | ã                                       | ار ۷ <u>ه</u>  | 5 N.                    | ပ<br>Z  | СНАЧ  |
| ф<br>ф  |   | 27.80<br>0.17.80<br>1.17.90  | ROUT                    | UNA UK  | にはなると<br>ではなるとしまれ   |
| 4<br>4  | 0 V 0                                   | 25<br>25<br>25<br>25<br>25<br>25<br>25<br>25<br>25<br>25<br>25<br>25<br>25<br>2                    | HJV.                    | ASTES TOUR NOT  | A SAN T   |
| **  | 00000000000000000000000000000000000000  | OUTPUT CONTROL VARIABLES 3 PRINT CONTROL 1FLOT 0 PLUT CONTROL 65CAL 0. HYCROGRAPH PLOT SCALE       | HYDROGRAPH ROUTING DATA | STURAGE POUTING NSTRS 11YP RSVAIC   | NORMAL DEPTH CHANNEL 10.01136  ANCH 0.050 NAIN CHANGE N-VALUE ANCH 0.050 NAIN CHANGE N-VALUE ANGH 0.050 KEANT N-VALUE RENTH 108050 ENERGY SLEDE ELMAX 0.050 ENERGY SLEDE  |
| & & & & & & & & & & & & & & & & & & &                     | 0 0 0                                   | C  | Η¥Ω                     | Vi  | Z   |
| ф<br>ф  | 0 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 |  |                         |   |   |
| #<br>#  | ×                                       | D  |                         | 'n  | U   |
| 0   | м<br>4<br>Ж                             | 35 KO  |                         | 36 85   | 37 FC   |
| ü   |   |  |                         |   |   |

| 60<br>60<br>74<br>74        | ELEVATION<br>GISTANCE                    |                        | 15.00 125.00 2                    | CRUSS-SECTION<br>90<br>60 249.90   | 110N DATA<br>000 250.00                        | O 270.00                      | 0 5 00                              | _       | RIGHT DVF RBANK 345.00 520. | 100             |          |
|-----------------------------|--|------------------------|-----------------------------------|--|--|-------------------------------|-------------------------------------|---------|-----------------------------|-----------------|----------|
|                             |  |                        |                                   |  |  | #<br>#                        |                                     |         |                             |                 |          |
| 67                          | STORAGE                                  | 91.31                  | 3.92                              | 171.28   | CUMPUTED STORAGE - OUTFLOW 11,77 222.84 262.13 | RAGE-001FL<br>15.11<br>262.13 | .AW CURVE<br>19.65<br>349.14        | 23.60   | 29.27                       | 42.23<br>596.54 | 62.91    |
| J                           | BUTFLAM                                  | 1644.62                | 34.22                             | 103.77   | 3753.43  | 303,34<br>4809,95             | 473.78                              | 7556.25 | 9277:75                     | 930.29          | 13492:73 |
| ELE                         | ELEVATION                                | 7.89                   | 6.09                              | 1.58   | 10.26  | 3.16                          | 3.95                                | 12:63   | 13.42                       | 14.21           | 15:00    |
| * *                         |  | 0 0                    | ***                               |  | ***  | 4                             | *                                   |         |                             |                 |          |
|                             |  | HYDROGRAPH<br>FOX PLAN | APH AT STATION                    |  | 45   |                               | ,                                   |         |                             |                 |          |
| PERK FLOM (CFS) 11597.      | 1114<br>000.44<br>000.00                 | (INCHES)               | 6-118<br>90709<br>14.294<br>4496. | MAX1 MUM 24-HR 29-HR 2007-2012-0-2012-0-201-0-20 | AVERAGE FLOW 10908.                            |                               | 99.50-HR<br>791.<br>20.681<br>6508. |         |                             |                 |          |
| PEAK STERAGE<br>12C-FT)     | ######################################   |                        | 6-42<br>494                       | MAXIMUM AVERAGE<br>24-HR<br>176.   |  | STOKAGE 99                    | 7.50-HR                             |         |                             |                 |          |
| PECK STAGE (FILT) .         | 4<br>(HR)<br>00.00                       |                        | 6-HR<br>13.25                     | MAX134UR<br>24-197<br>7-50   | 7.50 AVERAGE 72.72.72.75.50                    | 72-HK 99                      | 3.50-HR<br>2.17                     |         |                             |                 |          |
|                             |  | CUMULATIVE             | E AREA =                          | 5.90 50  | ¥**<br>¥                                       |                               |                                     |         |                             |                 | •        |
| ***                         |  | 404                    | ****                              |  | ***  | *                             | 참                                   |         |                             |                 |          |
|                             |  | HYDROGRAP<br>FOR PLA   | AN 1. SATIOM                      | 110H 0.50  | 45   |                               |                                     |         |                             |                 |          |
| PEAK FLOW<br>(CFS)<br>5751. | TI 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | (INCHES)               | 6-HR<br>44966<br>7-085<br>2220    | MAXIMUM A<br>24-14<br>1601<br>10-002<br>3176   | AVERAGE FLOW<br>545.<br>2 10.309               | <u>ę.</u>                     | 7.50-HR<br>395.<br>10.350<br>3257.  |         |                             |                 |          |
| PERK STORAGE (AC-17)        | 111.<br>111.<br>11.00                    |                        | 6-HX<br>263.                      | MAXIMUM AVERAGE<br>24-HR<br>92.  |  | 72-HR 99                      | 99.50-HR<br>23.                     |         |                             |                 |          |
| PEAN STAGE<br>IFLET)        | 117E<br>148.00<br>14.00                  |                        | 6-9K<br>10.75                     | MAX1MUM AVE<br>24-HR<br>5.71   | RAGE   | 72-HK 99                      | 1.50-HR<br>1.60                     |         |                             |                 |          |
|                             |  | CUMULA TI VE           | E AREA =                          | 5.90 50  | Σ<br>11  | •                             |                                     |         |                             |                 |          |
| 440                         |  | 000                    | ***                               |  | <b>\$</b>                                      | ***                           | ŧ                                   |         |                             |                 |          |

| •      |   |  | •   |  |                   |             |                              |  |   |  |
|--------|---|--|---|--|-------------------|-------------|------------------------------|--|---|--|
| &<br>& |   | 99.50-HR<br>198.<br>5.175<br>1629.                       | 99.50-HK                                      | 99.50-HR<br>1.15                               |                   | ***         |                              | 99.50-HR<br>79.<br>2.071<br>652.   | 99.50-HR                                | 99.50-HR<br>0.70                         |
| ***    | 11CH A5   | MAXIMUM AVERAGE FLUM<br>24-HR<br>5-03-<br>1565-<br>1565- | MAXIMUM AVERAGE STORAGE<br>24-HR 72-HR<br>16. | MAXIMUM AVERAGE STAGE<br>24-HR<br>4-25<br>1-56 | 5.90 Sp MI        | ***         | 115N A5                      | MAXIVUM AVERAGE FLOH<br>72-HR<br>72-HR<br>2-010<br>5-010<br>6-99         | MAXIMUY AVERAGE STOKAGE<br>24-HR<br>16. | MAXIMUM AVERAGE STAGE                    |
| 330    | AT STA  | 200 H<br>100 H<br>100 H<br>100 H<br>100 H                | 6-HR<br>130.                                  | 8-57<br>5-67                                   | AREA =            | 3<br>4<br>9 | AT STA                       | 8 4 4 8 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4                                  | 6-HX<br>42.                             | 6-HZ                                     |
| 944    | HYDROGRAPH AT STATIGN<br>FOR PLAN 1. KATIO = 0.25 | (1NCHES)<br>(AC-FT)                                      |   |  | CUMULATIVE AREA = | ***         | HYDROGRAPH AT STATION - 0.10 | (1NCHES)<br>(AC+FT)  |   |  |
|        |   | 11.<br>11.<br>12.<br>10.<br>10.                          | 11 ME   | 111<br>6.00<br>00<br>00                        |                   | ,           |                              | HEO<br>THO<br>THO<br>THO<br>THO<br>THO<br>THO<br>THO<br>THO<br>THO<br>TH | 1114<br>64.00                           | #<br>E.E.E.E.E.E.E.E.E.E.E.E.E.E.E.E.E.E |
| 6 0 0  |   | FEAN FLOW<br>(CFS)<br>(2034)                             | PEAK CHTPAGE<br>(ACLET)                       | PEAK STAGE<br>(FEET)<br>9.41                   |                   |             | •                            | FEAK FLOW<br>(LFS)<br>1125.  | FEAK STEPAGE<br>(4C-FT)<br>5C.          | PEAK STAGE<br>(FEET)<br>6.83             |

5.90 SG MI

CUMULATIVE AREA =

|        | 000000000000000000000000000000000000000 | ###################################### |   |
|--------|---|--|---|
| 40 P.K | ÞΦ                                      | Af. 0                                  | DEVELOP LOCAL INFLOW HYDROGRAPH - BASS LAKE TO BLAIR LAKE |
|        | 0                                       | <b>e</b>                               |   |
|        | 200000                                  | ************                           |   |

SUPPASTA RUNDEF DATA

BASE FLOW CHARACTERISTICS INITIAL FLOW RECESSION EXCESS 15.00 BEGIN HASE FLOW RECESSION FILSK 1.00000 RECESSION CONSTANT SUPPASSIV CHARACTERISTICS TAREA TAREA 41 (.A 42 EF

| _  |   |                 | 671. 598.<br>7. 56.  |  |                   |   |                               |                                     |   |
|--|---|-----------------|--|--|-------------------|---|-------------------------------|-------------------------------------|---|
| E  |   |                 | 68APH<br>D 020 TA 707 5<br>91 •  | 49.50-HP<br>20.675.<br>2560.   | 3<br>0            | 99.50-HR<br>676.<br>20.851<br>5560.             | †<br>†<br>†                   | 99.50-HR<br>938.<br>10.425<br>7760. |   |
| INUL A PRECIPITATION TEANSPOSITION CUEFFICIENT TEANSPOSITION AREA USE SEG DISTRIBUTION CLF 17410. 300022116 IN GIVE  | INITIAL LOSS<br>UNIFORM LOSS RATE<br>PERCENT IMPERVIOUS ARFA  |                 | 1450. 34 END-OF-PERIODGE 165. 147. 116. 116. 110.  | MAXIMUM AVERAGE FLUH<br>24-118<br>20-20-20-20-20-20-20-20-20-20-20-20-20-2 | -                 | * × × ×   | λαφ<br>3N<br>8 0.50           |                                     |   |
| 10000 H  | 6 1 5 0 1 1 2 0 0 1 2 0 0 1 2 0 0 1 2 0 0 1 2 0 | UNITGRA<br>3.16 | 226.<br>235.<br>1.<br>2.   | 7 6-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1                                  | A T 4             | 200-4-200-4-3-4-4-4-4-4-4-4-4-4-4-4-4-4-4-4-4-4 | SAS.<br>H AT STATION          | 39759<br>39759<br>1971<br>1971      | : |
| ATTON DA<br>PREATING<br>SEPC<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>SECTO<br>S | ZA I  |                 | 130.<br>295.<br>27.  | (INCRES)<br>(ACHES)<br>(ACHES)<br>CUMULATIVE                               | ###<br>HYDEGGAAPH | (INCHES)<br>(ACAFT)<br>(U'ULATIVE               | ###<br>HYDFUGRAPH<br>FOR DIAN | (INCHES)<br>(INCHES)<br>CUMULATIVE  | • |
| PRECIPIT PRINABLE TE TR  | UNIFO   | scs o           | 4<br>4<br>4<br>4<br>6<br>6<br>6<br>7<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8 | ######################################                                     |                   | 1 HR<br>HR<br>00.00                             |                               | 4 (HZ)                              |   |
| £ .  | 21 :  | - 02 54         | •  | PEAK FLOW<br>(CFS)<br>10401.   | ¢ \$ \$           | PEAK FLUK<br>ICFS)<br>ICFOI.                    | 0<br>0<br>0                   | PEAK FLOW (CFS) 52.60.              | • |

506.

| A<br>0           |          |
|------------------|----------|
|                  | ر<br>د ک |
| 21 K 1 1 1 2 1 2 | h4110 =  |
| 4                | -        |
| CAAPH            | FUR PLAN |
| HYPRI            | F.C.     |

| FEAK FLOW (CTS) 2000.       | A STATE OF THE O | (CFS)<br>(1NCHES)<br>(AC-FI)<br>CUMULATIVE        | 6-HR<br>1957.<br>3.690.<br>986. | MAXIMUM AVERAGE FLOW<br>24-HK<br>24-HK<br>232<br>5-072<br>5-181<br>1353-<br>5-00 50 MI | 99.50-HR<br>169.<br>5.213<br>1390. |
|-----------------------------|--|---|---------------------------------|--|------------------------------------|
| 0                           |  | \$0 <b>0</b>                                      | 8<br>3<br>4                     | ***  | ***                                |
|                             |  | HYDROGRAPH AT STATION<br>FUR PLAN 1. RATIO * 0.10 | AT STATI                        | GN 0.10 A6   |                                    |
| FEAK FLOW<br>(OFS)<br>1040. | TIME<br>3.00   | (CFS)<br>(1vCHES)<br>(AC-FT)                      | 1775.<br>1.9776.<br>1.9976      | MAXIMUM AVERAGE FLOW 24-HR 24-HR 72-HR 2-629 2-629 5-53-                               | 99.50-HK<br>68.<br>7.085<br>556.   |
|                             |  | CUMULATIVE  | AKEA =                          | 5.00 SG MI   |                                    |
|                             |  |   |                                 |  |                                    |

ورق جوج فجو فجو جوب خوب خوب خوب خوب مور غوب مون عون جون مون مون عون مون هون هون هون هون هون مون مون مون مون هوه هوه

| ### COMBINE HYDROGRAPHS TO GET TOTAL INFLOW TO BLAIR LAKE ####################################   |
|--|
| ### COMBINE   CO |

\*\*\*

000

000

6. 0.

| 0<br>0                       |                               | £ 9 9   | 0 0   |  | ÷ ;  |                                   | ф<br>ф                             |  |  |                       |  |   |
|------------------------------|-------------------------------|---|---|--|--|-----------------------------------|------------------------------------|--|--|-----------------------|--|---|
| PEAK FLGH<br>(CTS)<br>(STS)  | 11<br>0<br>0<br>0<br>0        | HYDRUGKAPH<br>FG2 PLAN<br>(INCHES)<br>(AC-FT)<br>CUMULATIVE                     | A H   | FIG 8 0 . 2 . 2 . 2 . 2 . 2 . 2 . 2 . 2 . 2 .                          | 5 A 7<br>                                  | 7<br>72-UM<br>5055<br>3003.       | 99.50-HR<br>367.<br>3618.          |  |  |                       | ·                                      |   |
| <b>6</b><br>↔                |                               | ACC<br>HYDRUGRAFH<br>FOR PLAN   | A   | ATICH 0.10   | ***<br>0                                   |                                   | *<br>*                             |  |  |                       |  |   |
| FEAK FLOW<br>(2FS)<br>(2085. | 4<br>11.<br>10.<br>10.<br>10. | (1NCHES)<br>(ACCHES)<br>(UMULATIVE  | 1000 HK<br>1000 HK<br>1100 H | МАХІЗ<br>24<br>25<br>10 - 90   | VERAGE                                     | 7 FLUH<br>72-148<br>2-057<br>1202 | 99.50-4R<br>147.<br>2.017<br>1209. |  |  |                       |  |   |
|                              |                               | \$<br>\$<br>\$  | ene con e   | aca odo coc<br>Inflow Hydro  | * * * * K                                  | i¢a so¢ oo¢ e¢<br>THRNUGH BLAIR   | o one ene                          | ************************************** | ************************************** | 0<br>0<br>0<br>0<br>0 | ************************************** | • |
| 6 9 A S                      | ST04                          | HWARUGRAPH ROUTING STURAGE ROUTING STURAGE ROUTING                              | DATA<br>STOR  | NUMBER OF  | OF SURKEACHES IN                           | JES<br>HODITION                   |                                    |  |  |                       |  | •                                       |
| 52 5V                        | :<br>:                        | RSVRIC<br>X<br>STORAGE  | 2.00<br>0.00<br>0.00  | KKING<br>KKING<br>24.0   | COND 14 10N<br>AND 0 COE<br>30.0           | 40.0                              | 0.09                               | 80.0                                   | 109.0                                  | 142.0                 | 193.0                                  | 235.0                                   |
| 53 56                        | ELEV                          | ELEVATION   | 340.70  | 355.00   | 356.00                                     | 357.00                            | 359.00                             | 361.00                                 | 363.00                                 | 365.20                | 368.00                                 | 370.00                                  |
| 50 50                        | 0130                          | DISCHARGE   | •   | •  | 123.                                       | 348.                              | 986                                | 2253.                                  | 4122.                                  | 6746.                 | 13345.                                 | 21421.                                  |
| 51 SE                        | ELEV                          | ELEVATION   | 340.70  | 355.00   | 356.00                                     | 357.00                            | 359.00                             | 361.00                                 | 363.00                                 | 355.20                | 368.00                                 | 370.00                                  |
| \$ 28                        | 1148                          | SPILLHAN<br>SON<br>SON<br>SON<br>SON<br>SON<br>SON<br>SON<br>SON<br>SON<br>SO   | 80<br>60<br>60<br>60<br>60<br>60<br>60  | SPILLWAY CREST<br>SPILLWAY WIDTH<br>HEIR COEFFICIEN<br>EXFONENT OF HEA | CREST ELE<br>MIDITH<br>FFICIENT<br>OF HEAD | ELEVATION<br>T<br>D               |                                    |  |  |                       |  | •                                       |
| 55 51                        | 100                           | FC<br>FC<br>FC<br>FC<br>FC<br>FC<br>FC<br>FC<br>FC<br>FC<br>FC<br>FC<br>FC<br>F | 359<br>599<br>500<br>100<br>100   | ELEVATION AT<br>DAM WIDTH<br>WEIR COEFFICI<br>EXPONENT OF H            | TOP<br>EAD                                 | OF DAM                            |                                    |  |  |                       |  |   |
|                              |                               |   |   |  |  | ¢                                 |                                    |  |  |                       |  |   |

**\*** 

| -  |  |
|----|--|
| ٠. |  |
|    |  |
| w  |  |
| -  |  |
| v  |  |
|    |  |

.

.

| • | 193.60 235.00             | 0 13345.00 21421.00 | •         |                        |                 |                                       |  |   |            |     | •                      |                 |  |                                 |   |            |             |
|---|---------------------------|---------------------|-----------|------------------------|-----------------|---------------------------------------|--|---|------------|-----|------------------------|-----------------|--|---------------------------------|---|------------|-------------|
|   | 142.00                    | 6748.00             |           |                        |                 |                                       |  |   |            |     |                        |                 |  |                                 |   |            |             |
|   | 109.00                    | 4122.00             |           |                        |                 |                                       |  |   |            |     |                        |                 |  |                                 |   |            |             |
|   | FLOW CURVE<br>80.00       | 2253.00             | ***       |                        |                 | 99.50-HR<br>1467.<br>20.756<br>12066. | 99.50-HR   | 99.50-HR<br>357.02                          |            | *** |                        |                 | 99.50-HR<br>734.<br>10.383<br>6035.    | 99.50-HR<br>39.                 | 99.50-HR<br>356.43                      |            | <b>*</b>    |
| * | ORAGE -DUT                | 984.00              | ī         |                        |                 | 3E FLOW<br>2019:<br>2019:<br>12011:   | STORAGE<br>72-HR<br>54.  | F STAGE 357.73                              | •          | 7   |                        | ı               | 10533<br>1007•                         | 510RAGE<br>72-HR                | SE STAGE 356.95                         |            |             |
|   | COMPUTED STORAGE -DUTFLOW | 348.00              | <b>\$</b> | 884                    |                 | VERA(                                 | MAXIMUM AVERAGE S  | AVERAGO                                     | I F        | *   | 0 48                   |                 | IVERAG                                 | 24-HR 3                         | VERAC                                   | So MI      | *           |
|   | 30.00                     | 123.00              |           | STATION . KATIO        | IOURS           | MAXIMUM 24-HR 592B- 20-228 11759.     | MAXIMU.  | •   | 10.90 50   |     | STATION 8 0.50         | IDURS           | MAXIMUM 24-11R 29-51:<br>100-101 5672. | MAXIMUY                         | MAX IMUM A 24-HR 340.29                 | 10.90      |             |
|   | 24.00                     | 0.0                 | *         | 4-                     | 43.50 HOURS     | 6-HK<br>16750-<br>14-513              | 6-HR<br>210.   | 368.7                                       | E AKEL =   | 000 | A 1                    | 43.50 HDURS     | 8301H<br>4109004<br>4172               | 6-HK<br>153.                    | 365.73                                  | E AREA =   | 6<br>6<br>6 |
|   | 0.0                       | 0.0                 | £ \$      | HYDROGRAPH<br>FOR PLAN | 21554. AT TIME  | (INCHES)                              |  |   | CUMULATIVE | 400 | HYDRUGRAPH<br>FOR PLAV | 10652. AT TIME  | (INCHES)                               |                                 |   | CUMULATIVE | <b>\$</b>   |
|   | STURAGE                   | GUTFLOW             |           |                        |                 | 1112<br>CHR<br>02.50<br>00            | 4<br>3<br>3<br>3<br>5<br>5<br>6<br>7<br>7<br>7<br>8<br>7<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8<br>8 | # CHE * C * C * C * C * C * C * C * C * C * |            |     |                        |                 | 1114<br>(HR)<br>13:50                  | 1114<br>(HP)<br>43.50           | 4 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 |            |             |
|   | ••                        | J                   | 40        |                        | FEAK CUTFLOW IS | PEAK FLUN<br>(CFS)<br>21554.          | PEAK STOTAGE<br>(AC#FT)<br>(30.  | PEAK STAGE<br>(FEET)<br>370-63              |            | 644 |                        | FEAK GUTFLOW IS | PEAK FLOW<br>(CFS)<br>10652            | PEAK STOPAGE<br>(AC-FT)<br>172. | PEAK STAGE<br>(TEFT)<br>310-55          |            | <b>Q</b>    |

| 90°0    | IATITUS SE AB         |
|---------|-----------------------|
| 544     | HYDROGRAPH AT STATITU |
| 404 404 | •                     |

| EAK GUTFLGW 15                         |   | 70 4 5 C C C C X 7                                | AT STAT                              | 11.11   |                           |
|--|---|---|--------------------------------------|---|---------------------------|
| FEAK CUTFLOW IS                        |   | FUR PLAN I. KATIO = 0.25                          | 1. KA11                              |   |                           |
|  |   | 5226. AT TIME 43.50 HIUAS                         | 43.50 HD                             | 24.5  |                           |
| FERF FLON (5.25)                       | 1118<br>63.50<br>500<br>500<br>500<br>500 | (1NC)<br>(1NC)<br>(1NC)<br>(1NC)                  | 6135<br>2055<br>2055<br>1055<br>1055 | MAXIMUM AVERAGE FLUM<br>1477-<br>1477-<br>5-041-<br>2931- | 99.50-HR<br>3671<br>30191 |
| PEAK STFKAGE 7 (123-43)                | 1127<br>(HP)<br>63.50                     |   | 103.                                 | MAXIMUM AVERAGE STORAGE 24-HR 24-HR 60.                   | 99.50-HR                  |
| PEAK STAGE T<br>(FEET) 63<br>363.93 63 | 11.84<br>63.50                            |   | 6-H2<br>362.93                       | MAX1MUM AVERAGE STAGE<br>24-HR<br>358.72 356.34           | 99.50-HR<br>355.98        |
| •                                      |   | CUMULATIVE SKEA =                                 | JREA =                               | 10.90 SG MI   |                           |
| **                                     |   | <b>\$</b>   | ***                                  | ***   | 6 4 6                     |
|  |   | HYURUGRAPH AT STATICN<br>FUR PLAN 1. RATIU * 0.10 | AT STAT                              | 1CN 48  |                           |

99.50-HR

MAXIMUM AVERAGE FLOH
24-HR
24-HR
72-HK
702,
25010
1169.
1169.
RAXIMUM AVERAGE STORAGE
43.

2074. AT TIME 43.50 HOUES

PEAK CUTFLOW 15

PEAK FLUM ICES)

99.50-HR

MAXIMUM AVERAGE STAGE 24-HF 357-22 355-78

10.90 SO MI

360.05 CUMULATIVE AREA =

PEAK STERAGE TIME (HR) (AST) (

PEAK STERAGE

PEAK FICH AND STAGE (END-DF-PEKION) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS

| CFERATION     | STATION  | AREA  | PLAN            | Œ                               | RATIO 1                    |                       | APPLIED FRATIONS RATIONS | RATIOS APPLIED TO FLOWS<br>RATIO 2 RATIO 4<br>0.53 0.13 |  |
|---------------|----------|-------|-----------------|---------------------------------|----------------------------|-----------------------|--------------------------|---|--|
| HYDREGUAPH AT | Al       | 5.90  | -               | FLOW                            | 12000.                     |                       | 3000.                    | 1200.   |  |
| FEUTED TO     | A2       | 5.90  | -               | FLGW<br>TIRE                    | 11982.                     | 5987.                 | 2487.                    | 1185.   |  |
|               |          |       | <b>⇔</b><br>₩ • | PEAK STAGES<br>STAGE<br>TIFE    | 1N FEET<br>110.83<br>43.00 | 107.58                | 135.55                   | 103.64  |  |
| REUTED TO     | A3       | 5.90  | H               | FLC8                            | 11980.                     | 5989.<br>43.00        | 2984.                    | 1186,   |  |
| •             |          |       | 44              | PEAK STAGES IN FEET STAGE 13.14 | 1N FEET<br>13.14<br>43.00  | 44<br>9.91<br>43.00   | 43.00                    | 43.50   |  |
| ACUTED TO     | P P      | 5.90  | -               | FLCW<br>TINE                    | 11910.                     | 5952.<br>43.00        | 2376.                    | 1188  |  |
|               |          |       | 7 4             | PEAK STAGES I<br>STAGE<br>TIME  | 18 FEET<br>18.21<br>43.00  | ##<br>13.57<br>43.00  | 10.28                    | 6.67<br>43.50   |  |
| ROUTED TO     | . A5 .   | 2.90  |                 | FLOW<br>11 ME                   | 11597                      | 5751.                 | 2834.<br>44.00           | 1125.   |  |
|               |          |       | ф. <b>-</b> -   | PEAK STAGES IN FEET STAGE 14.33 | IN FEET<br>14.33<br>44.00  | 44.00                 | 9.41                     | 6.83  |  |
| HYDRCCRAPH AT | <b>9</b> | 2.00  | -               | FL C.W<br>11 NE                 | 10401.                     | 5200.                 | 2600.                    | 1040.   |  |
| 2 COPEINED AT | LA       | 10.90 | <b>~</b>        | FLCW<br>TIME                    | 21537.                     | 10659.                | 5246.<br>43.50           | 43.50   |  |
| מבטזננ זם     | A 8      | 10.90 |                 | FLOW                            | 21554                      | 10652                 | 5726.                    | 43.50   |  |
|               |          | ·     | 7 .             | PEAK STAGES<br>STAGE<br>TIME    | 1N FEET<br>370.03<br>43.50 | **<br>366.86<br>43.50 | 361.93                   | 360.72  |  |

SUMMARY UF DAM OVERTOPPING/HREACH ANALYSIS FOR STATION

|                                       | TIME OF<br>FAILURE<br>HOURS      | 0000   |
|---------------------------------------|----------------------------------|--|
| 100 0F 0AM<br>359.00<br>50.00<br>984. | TIME DE MAX OUTELOW HOURS        | 4444<br>WWWW<br>PANNO<br>OOCO                                |
|                                       |                                  | 115.50   |
| SPILLHAY CREST<br>3:5.00<br>24.       | MAX 1 PUM<br>OUTFL JW<br>CFS     | 21554<br>10659<br>5658<br>2076                               |
|                                       | MAXINUM<br>STURAGE<br>AC-FT      | 236.<br>123.<br>77.  |
| 141714L VALUE<br>355.00<br>24.        | MAXIMUM<br>DEPTH<br>OVER DAM     | 11.03<br>7.93<br>4.93  |
| FLEVATION<br>STOPAGE<br>DUTFLOA       | MAYINCM<br>RESERVOIR<br>W.S.ELEV | 8889<br>8886<br>8886<br>8888<br>8888<br>8888<br>8888<br>8888 |
|                                       | A TIO                            | 1009<br>3004<br>0000   |
| FLAN 1                                |                                  | •  |

eee HURMAL END OF JOB 600

| 10        |  |                          |  | 21421.                          | 370  |                  |   |  |
|-----------|--|--------------------------|--|---------------------------------|--|------------------|---|--|
| .6        |  |                          |  | 13345                           | 368  |                  |   |  |
| 8         | JENSHIP  |                          |  | 6748.                           | 365.2  |                  |   | 1020.  |
| 7.        | STOWN TO   | -                        | KE   | 4122                            |  |                  | OXN   | 520.1 770. 1020.                                 |
|           | CN GOOGH   | .966                     | ELAIR LA                                   | 2253                            | 361.   |                  | ELAIRST                                     | 520.1<br>6.                                      |
| · · · · · | SIS<br>COUNTY  | 940.                     | нуповн.                                    | 984<br>355                      |  | 359.             | THROUGH                                     | 520<br>011                                       |
|           | SLAIV LAKE DAN BELACH ANALYSIS ICM GOOCH ANCO SEN JERSLY DAN NC. 774 - MACREN COUNTY - BLAIRSTOWN TOWNSHIP Z 1 1 | ROGEAPH<br>980.          | ROUTE INFLOW HYDROGRAPH THROUGH BLAIR LAKE | 34<br>37<br>57                  | 845<br>845<br>845<br>845<br>845<br>845<br>845<br>845<br>845<br>845 | 0                | RCUTE GUTFLOW HYDROGRAPH THROUGH BLAIRSTOWN | 840<br>5000                                      |
|           | 841.8<br>0 774   | IR.PUT INFLOW HYDROGEAFH | FLCM SYD                                   | C<br>M<br>M<br>C<br>M<br>M<br>M | 1977<br>1978<br>1979<br>1979                                       | 0 0<br>0 0       | TELON HY                                    | 980.<br>10<br>499.9<br>6.                        |
|           | LAKS DAM<br>RSLY DAM   | #.701<br>1906            | ROUTE IN                                   | 7 8<br>1 8<br>1 8<br>1 8<br>1 8 | и<br>1502<br>1504<br>1504  | ง.<br>ง.บ<br>ง.ค | RCUTE, CU                                   | 7 000 m  |
|           | 2011<br>A 11<br>A 12<br>D 11 4   | 980.                     | 4  | 340.7                           | 340.7  | 340.7            | 300   | <br>   |
| 10.       | 00-0   | χυ<br>Συ                 | XX:  | now.                            | さしい  | 1-E              |   | CKE WIEN<br>CKE WIEN                             |
|           |  |                          |  |                                 |  |                  |   | •  |
| 113       | HORIS  | N-D                      | <b>~</b> w                                 | () ( () pin (<br>pin() = ()     | CALA<br>Temper   | Uid.             | 17  | いいむentys<br>・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・ |
|           |  |                          |  |                                 |  |                  |   |  |

THE HYDRULUGIC LUCINELRING CENTER 609 SECEND STREET 609 SECEND STREET 616) 440-3285 CR (FIS) 448-3285

BLAIR LAKE DAN BREACH AMALYSIS TOB GOOCH ANGO HEB JERSEY DAN ME. 774 - DARREN COUNTY - ELAIRSTOWN TOWNSHIP

CUTPUT CENTROL VARIABLES PRINT CONTROL IPENT I PLOT CONTROL IPENT CONTROL IPENT CONTROL CALE CALE CALE PRINT CIACNOSTIC MESSAGES

HYGRCGRAPH TIME DATA 1 MIMUTES IN COMPUTATION INTERNAL 104 PT 104 PT 105 
\_

NUTIBE 1 CORP. ENGING TIME COMPUTATION INTERVAL 0.02 HOURS

ENGLISH UMITS
PRECIPITATION DEPTH INCHES
PRECIPITATION DEPTH INCHES
ELST FLEVATION CUBIC PEET PER SECOND
STAFFACE VOLUME ACKES FAHRENHEIT

SURBASIN PUNGFF DATA
SUBBASIN CHARACTERISTICS SUPBASIN ARFA

4. t. A

HYDROGRAFH AT STATION

| ****                                  | FLG       | 99090000000000000000000000000000000000  |                                    | **  |  |  |             |   | 235.0 | 370.00 | 21421.  | 370.00  |  |
|---------------------------------------|-----------|---|------------------------------------|---|--|--|-------------|---|-------|--------|---------|---------|--|
| ****                                  | 080       | **************************************  |                                    | **************************************  |  |  |             |   | 193.0 | 368.00 | 13345.  | 368,00  |  |
| ****                                  | MON PE    | \$305555555555555665566   |                                    | 0<br>0<br>0<br>0  |  | •  |             |   | 42.0  | 5.20   | 748.    | 5.20    |  |
| Ö                                     | OA        | ederalededededededededededededededededededed  |                                    | <b>*</b>  |  |  |             |   | -     | 36     | •       | . 36    |  |
| e<br>e                                | r e s     | 10000000000000000000000000000000000000  |                                    | *<br>*  |  |  |             |   | •     | 90•    | 5.      | 00•     |  |
| ****                                  | M.ITS     | 00000000000000000000000000000000000000  |                                    | # # # # # # # # # # # # # # # # # # #   |  |  |             |   | 109   | 363.   | 4122    | 363.    |  |
| *****                                 | C Y J     | らきまる はっちゅうしょう ままる しょくしょく しょく しょく しょく しょく しょく しょく しょく しょく  |                                    | *   |  |  |             |   | 80.0  | 361.00 | 2253.   | 361.00  |  |
| ******                                | MEN HEMB  | COCOCOCOCOCOCOCOCOCOCOCOCOCOCOCOCOCOCO  | 0000<br>0000<br>• 0000             | \$<br>\$<br>\$<br>\$  | A<br>K                                   |  |             |   | 0.09  | 99.00  | 984.    | 69.00   |  |
| 4<br>4<br>4                           | 2.        | ;<br>; — — — — — — — — — — — — — — — — — —  |                                    | Ф<br>Ф  | ب<br>۲۲                                  |  |             |   |       | m      |         | L.)     |  |
| 4<br>4<br>4<br>4<br>4                 | ្រួ       | ********************************  | _                                  | *<br>*<br>*   | BLA:                                     |  |             | TION  | 0     | • 00   | ,<br>8, | 00.     | z                                      |
| 55.50                                 | E         |   | : πνν.<br>: πιποα<br>: πποο        | *<br>*<br>*   |  | <u>ن</u><br>ننا  |             | <u> </u>  | 4     | 357    | K)      | 357     | VATION                                 |
| 0000                                  | Ξ         | ල් ප්රතිශ්ර ප්රති ප්රතිශ්ර ප්රති ප්රතිශ්ර ප්රතිශ්ර ප්රතිශ්ර ප්රතිශ්ර ප්රති ප්රති ප් | . S                                | #<br>#<br>#   | Тнквисн                                  | SCAL   |             | ACHES<br>COND<br>CEFF   | 0     | Ó      | •       | 0       | FLEV<br>AD                             |
| · · · · · · · · · · · · · · · · · · · |           | *   | . V E                              | 6<br>*<br>*   | GRAPH                                    | ROL<br>GLOT  |             | 01-00<br>11-01-00<br>11-11-11-11-11-11-11-11-11-11-11-11-11-  | 30.   | 56.0   | 123     | 56.0    | OCO<br>PEER<br>PEER                    |
| 0000                                  |           | 日日日日にはこれなることできまっている。 ポート・ロード・ファイン・ファイン・ファイン・ファイン・ファイン・アー・アー・アー・アー・アー・アー・アー・アー・アー・アー・アー・アー・アー・   | + N40. •<br>- D1000 N<br>- N7000 G | 65<br>66  | CD<br>Gr.                                | 224<br>240<br>440  |             | 0 - 0<br>E - 0<br>504<br>NHSN   |       | w.     |         | и,      | >>==================================== |
| 6 6 6 6<br>6                          | Ë         | 1 000000000000000000000000000000000000  | × 0                                | 40<br>40<br>40<br>40  | нүө                                      | 717<br>700<br>700<br>700<br>700<br>700<br>700<br>700<br>700<br>700 |             | BER<br>THE<br>TARE  | 0.4   | 00.    | ં       | 00.     | 1180<br>2 TT<br>2200<br>3200<br>4403   |
| 4 10 12 4                             | Ξ.        | _ ಎಂಎಂಎಂಎಂಎಂಎಎಎಎಎ   |                                    | #<br>#<br>#   | F COX                                    | 90 ±<br>€ 3≻<br>ਜਹਾਹ   |             | SELON<br>SELON<br>CHAN<br>CHAN<br>CHAN<br>CHAN<br>CHAN<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON<br>SELON | (A    | 355    |         | 355     | SC SE                                  |
| · 电电子电                                | 115 V     | j<br>;<br>;<br>;<br>;<br>;  | : 1000 K                           | ∜<br>≎<br>₩<br>₩  | اب<br>د:<br>د                            | 50<br>50<br>6•   | <b>'</b> -a | 100<br>100<br>100   | 0     | O      | •       | c       | 0000<br>0000                           |
| 4 10 14 10                            | ۱.        |   | <                                  | *   | FOUT                                     | VARIA  | DAT         | 980   | ò     | 40.7   | C       | 40.7    | 5 64<br>5 64<br>6 440 64               |
|                                       | জনা ব     | 1   | 200 5                              | \$*<br>\$*<br>\$*<br>\$*  |  | מר א   | -           | 116   |       | Ŕ      |         | ď       |  |
| )<br>)<br>)                           | F. C. 18  | 000000000000000000000000000000000000  | ( O50 2                            | ē.  | 10 40 40 40                              | 2000<br>1001<br>1001<br>1001                                       | Œ           | A POOL POOL POOL POOL POOL POOL POOL POO  | L     | 7      | 1.4     |         | 1027<br>1040<br>1040<br>1071           |
| •                                     |           |   |                                    | # #<br># #<br># #<br># #<br># #   | 12 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | 0220   | FAPH        | 20E 102 1   | CFAC  | NOIT   | JO.AV.  | Ĺ.      | マーマンド・                                 |
| :                                     | נוגנ      | ₹   | , u,-r                             | \$ \$\\ \text{\$\delta}\$ \$\\ | 24444444                                 | OUTFUT   | <u>ن</u> .  | STURY   | 21.0  | LEVATI | DISCHAF | ELCVATI | SPILLS                                 |
| 3                                     |           |   | I.E.                               | \$ . \$<br>\$ . \$<br>\$ . \$<br>\$ . \$  | 0000                                     |  | HYL         |   |       | u.     | <i></i> | u.J     | •                                      |
| )<br>)                                | i de la   | HERMONDOSOSOS   | \$<br>\$<br>\$                     | 0 0<br>0<br>0   | <u> មក្ខភ្នំ</u>                         |  |             |   |       |        |         |         |  |
| \$<br>2<br>2                          | ` <u></u> |   |                                    | #<br>#<br>#   | X<br>X                                   | <u>ي</u><br>پر   |             | Š   | A)    | ъ,     | بن      | u.      | S                                      |
| :                                     | ٠.<br>٤.  | ्रे<br>- स्वस्थानम्बर्गास्थान्त्रेर्यस्थान्त्रेर्यस्थान्त्रेर्यस्थान्त्रेर्यस्थान्त्रेर्यस्थान्त्रः<br>- दे   |                                    | မ<br>မ  | ٠<br>۲                                   | 80   |             | c.<br>a.  | 2.5   | 13 5   | 10 2    | 11 :    | গে<br>জ<br>ল                           |
| •                                     |           | 4   | . a.                               | •   |  |  |             |   |       |        |         |         |  |

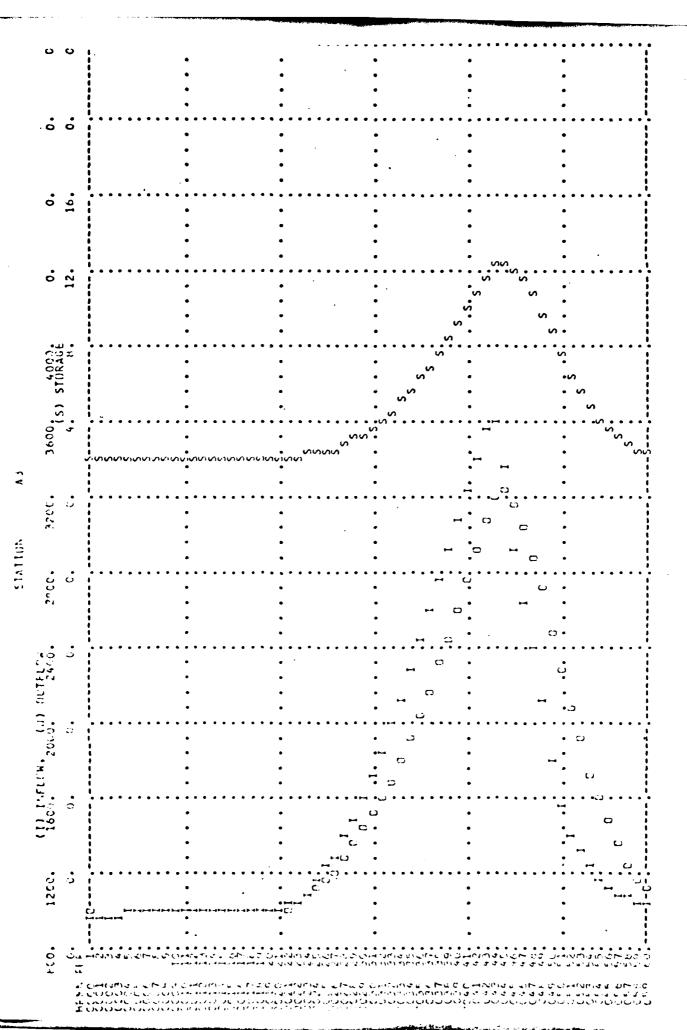
|  |  |              |              | 41<br>41<br>41                           |               | <b>ታ</b><br>ቁ                         | STA     | መመጠጠጠጠጠጠጠጠጠጠጠጠጠጠጠ<br>የተነንደ ተቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀቀ  | ***                                    |  |                                       |  |
|--|--|--------------|--------------|--|---------------|---------------------------------------|---------|---|--|--|---------------------------------------|--|
|  |  | 235.00       | 421.00       | ######################################   |               | 다<br>다<br>다<br>다                      | STORAGE | ころことともまままま<br>みまできららちらこうのみのからはおきをはなる。<br>なまちがかのでほどままできるできなられる。  | ***                                    | ,  |                                       |  |
|  |  | 00           | co 21        | 4<br>4<br>4<br>4                         |               | 4):<br>4):                            | TFLOW   | ままちょうとうしょうしょうしょうとうできません しょうしょうしょう しょうしょう しょく ちょく かいて ようきょう しょう かいしょ かん ちょう しょう しょう しょう しょう しょう しょう しょう しょう しょう し  | ***                                    |  |                                       |  |
|  |  | 193.         | 3345.        | 4<br>4                                   |               | ***                                   | 0       | しゅうしょうしょうしょうしょうしゅう  | ***                                    |  |                                       |  |
|  |  | 00•          | 00 1         | **************************************   | }<br>}<br>}   | ·<br>·                                | RWN OR  | 00300000000000000000000000000000000000  | *<br>*******                           |  |                                       |  |
|  |  | 142          | 6748         | 4  |               | ***                                   | NOW.    | 000000000000000000000000000000000000000   | 0<br>0<br>0<br>0<br>0                  |  |                                       |  |
|  |  | 00.          | 00           | 1<br>1                                   | )<br>}        | ě.                                    | ۷۵.     |   | \$<br>\$<br>\$<br>\$<br>\$<br>\$       |  |                                       |  |
|  |  | 109          | 4122.        |  |               | 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 |         | UUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUU  | *****                                  |  |                                       |  |
| •                                      | LURE   | LOW CURVE    | 2253.00      | 4  | 7.7           | ****                                  | STURAGE | られいららいころうらいらららられるようなす。<br>ひい うりゅうけん アーション・ラット・ラット・ラット・ラット・ラット・ラット・ラット・ラット・ラット・ラット   | · · · · · · · · · · · · · · · · · · ·  | 0.98+HK<br>1626.<br>0.000<br>132.  | C.98-HK                               | 0.98-HR<br>355.52                        |
| ж<br>С                                 | JE BREACT<br>DEVELOP<br>RISGER FAI   | 00.4GE -0UTF | 984.00       |  | STATIC        | ***                                   | ดบารเดน |   | <b>建设设备公司公司的公司</b>                     | 100-100-100-100-100-100-100-100-100-100  | ところ                                   | 25 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 |
| TOP OF                                 | 03:07<br>  | 500.         | 00.          | **************************************   | AP.H          | 다<br>다<br>다                           | ORC     | るるなどなるないないは、まないは、まなるは、まなるないとうなっているのできる。   | 요<br>요<br>요<br>&                       | SACE 7   | AGE ST                                | SAGE                                     |
| ارا<br>الم                             | 46664<br>FU 046<br>AN ACO<br>SOLOE<br>COLOE  | CHPUTE<br>40 | 348          | 7 00 00 00 00 00 00 00 00 00 00 00 00 00 | 50 50         | е<br>е                                | N. C.   | 00.00000000000000000000000000000000000  | ***                                    | A A VES  | 44 E B<br>3.                          | A 4 € 6                                  |
|  | A TOO SOLUTION OF THE SOLUTION | , 00°0       | 3.00         | +<br>+<br>+                              | ) I<br>}<br>} | \$<br>\$<br>\$<br>\$                  | NOW 4   |   | ***                                    | 21.000<br>21.000<br>21.000   |                                       | 11-02<br>11-02<br>11-02                  |
| ************************************** | >  | W.           | 12.          | 1  |               | **                                    |         |   | \$ 3.                                  | <b>2</b>   | ર                                     | કે.                                      |
| 1 5 U<br>20 10<br>0 0 0 A<br>0 0       | 05450<br>6500<br>6000<br>6000<br>6000  | 37.45        | ა <b>•</b> ც | 4<br>4<br>4                              |               | · · · · · · · · · · · · · · · · · · · | STAGE   | \$\$\text{\$\ | 0.72                                   | 6. •0 •<br>5. •0 •<br>5. •0 •<br>6. •0 •   | () •<br>() ()<br>• ()                 |  |
| M<br>Webu<br>Edwydd                    | 4100mm   | 0.0          | 0.0          | <u> </u>                                 |               | \$P\$ \$P\$ \$P\$ \$P\$               | STURAGE | ක්ක්ක්ක්ක්ක්ක්ක්ක්ක්ක්ක්ක්ක්ක්ක්ක්ක්ක්  | aaaaaaaaa<br>at time                   | 000<br>6001<br>6001  |                                       |  |
|  | EACH<br>PHI<br>FATE<br>FATE  | •            | J            | 0.28                                     |               | <b>你</b> 会会会会会                        | UTFLOR  | 2.3.2.2.2.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.  | 2132. I                                | ONI  |                                       |  |
| 10,                                    | u<br>u   | STOPAGE      | GUTFLOK      | L USE                                    |               | 於<br>삼<br>삼<br>삼<br>삼<br>4<br>4<br>4  | ים כאם  | 。<br>この 3 インスを見るというのの 10 できましました。<br>この 10 できましましました。<br>この 10 できましましましましましましましましましましま。<br>この 10 できましましましましましま。<br>この 10 できましましましましましま。<br>この 10 できましましましま。<br>この 10 できましましましま。<br>この 10 できましましま。<br>この 10 できましま。<br>この 10 できまと。<br>この 10 できまと。<br>こ           | , SI                                   | 11"E<br>(HE)<br>0.72   | i i i i i i i i i i i i i i i i i i i | 1000<br>200<br>144 1<br>1-000            |
| F                                      | รา<br>งา   |              | •            | 10 5 M F 4                               | *<br>\$<br>\$ | 60<br>60<br>60<br>60<br>60            | 2 XXX   | 0-mm/s/n/s/ms/0-mm/s/n/s/n/c/00/00/00/00/00/mm/mm/mm/mm/mm/mm/mm/mm/  | Addeseas<br>CUTFLOW                    |  | 210 46E<br>-FT)                       | S726E                                    |
| **                                     | 16   |              |              | - × 1                                    | e<br>}<br>}   | \$ 6<br>6<br>0<br>0                   | ያል ልያ ፡ | para mangad manani mina mina manana ay amina m  | ###################################### | 75<br>70<br>70<br>70<br>70<br>70<br>70<br>70<br>70<br>70<br>70<br>70<br>70<br>70 | ن<br>نو<br>نو<br>نو<br>نو             | 3112 U<br>31 2 C 1<br>41 2 C 1           |

are properties and an extension of the control of t

**各种种种种种种种种种种种的,是是一种种的,是是一种的,是是一种的,是是一种的,是是一种的,是是一种的,是是一种的,是是一种的,是是一种的的,是是一种的的的,是是是一种的的的,是是是一种的的的的,是是是一种的的的的,是是是一种的的的的,但是是是一种的的的的的,但是是是一种的的的的。** STAGE 004004-0040-4044 005004-4050-4044 005004-4050-4044 STORACE 7.58 1853.39 102.61 るるますますることできるようです。 するできるようにしょうです。 するもっていましょうでしょう するまちてきまるはするのので 3.14 1407.03 15.16 1112.57 DA MON HRMN RIGHT DVERBANK 11.00 770.00 1020 5.69 14918:05 59.07 5.05 \*\*\*\*\*\*\*\*\*\* 520.10 NCWMAL DEPTH CHARMEL REUTING OVERBANK N-VALUE
ANCH 6.040 NAIN CHARNEL N-VALUE
ANCH 0.010 NAIN CHARNEL N-VALUE
840. NAIOH CARE LEVE
SEL 0.0110 ENERGY ELEPE
1 LMAX 0.01 ENERGY ELEPE 4.21 CUMFUTED STORAGE - UUTFLOW CURVE 1-63 27:84 36:36 47:36 11596.59 **松 松** とうろうらうろうろきにはなる。 STURAGE CADSS-SECTION DATA
16.00 11.03 496.90 500.00 526.00 ROUTE CUTFLER PYDROSKAPH THROUGH PLAINSTOWN 40 40 40 PYDROGRAPH AT STATICA 化化 3.37 40.8498 8848.04 DUTFLOW Machaelman NOTE OF THITTAL CONDITION INTIAL CONDITION INTIAL CONDITION HOSELING R AND D CCEPFICIENT č G 於 存 於 PRINT CONTROL PLUT CONTROL HYDRUGRAPH PLUT SCALE 316.20 130 130 140 140 acaractariaca aractularibus midupataronum politicandus a . e ( . 000 7251 ZCS CHNESS SHED ON MICHAEL CONNESS ON COCCO TO JOSE OF COCCO TO JOSE OF COCCO TO JOSE OF 40 40 40 ं इ. 168.32 10.64 C C 40 14 15 CUIPUT CONTROL VARIABLES FROM VARIABLES FROM FOLDT CONTROL CON 71.08 980.00 € 0 0 % 0 0 0 0 3512.44 合 合 合 HYDROCFARM PROTING DATA **企**合作 STURACE FOUTING TANKS TANKS TANKS TANKS TO STANKS TO STA 증 수 수 2532.15 0.0 0.0 0.4 0.4 存分价 CUTFLOW FLEVATION かなか PUTFLOW C. G. ى بەرئىلىدىن ئەرىلىك ئا خاللانلىك ئارىلىلىلىلىلىلى からな DANMAINAMAA BAANAA QODGOO DE COURTAINA QODGOO DOO DOO DOO QODGOO DOO DOO DOO DOO ななな といる 400 **>-**>< **L**-u/ ŝ ũ 7. **ر** 7 25

3.5

| - 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0                     | 20000            |   |                        |                             |            |
|---|------------------|---|------------------------|-----------------------------|------------|
| NAMMA<br>NAMMAN   | ****             |   |                        |                             |            |
| 2000<br>2000<br>2000<br>2000<br>2000<br>2000<br>2000<br>200 | ***              |   |                        |                             |            |
| <b>ららららい</b> 。  | ***              |   |                        |                             |            |
| 00000<br>00000<br>00000<br>00000<br>00000                   | ***              |   |                        |                             |            |
| IAAAAA  | ***              |   | •                      |                             |            |
|   | ****             |   |                        |                             |            |
| **************************************                      |                  | 0.98-HR<br>1023.<br>0.000   | 0.98-HR                | 0.98-HK                     |            |
| Mericas<br>Manas<br>Genaras<br>Morenas                      | ****             | 7. FL Su<br>1.52.3.<br>1.32.3.  | \$108A66<br>72-HF      | 27.45<br>72-HF              |            |
| minimate<br>Turbin  | か<br>分<br>を<br>か | RAGE  | AGE                    | 3978.                       |            |
| 100 000<br>00000<br>00000<br>00000<br>00000                 | ****             | 24 - Hr AVERACE 72-15<br>1623 - 0.000<br>0.523 - 0.000<br>0.523 - 0.000       | MAXING AVERAGE SIBBAGE | MAXIVUN AVERAGE STAGE       | 1 × 05     |
| garante de la compania                                      | 0<br>0<br>0<br>0 | 3 4 4 6 A   | × a×                   | તે<br>દ                     | 0.0        |
| কককক<br>* * * * *<br>24 সমাজ                                | 00000000         | 1 40 4<br>2 400<br>3 44<br>4 40<br>4 40<br>4 40<br>4 40<br>4 40<br>4 40       | 6-1-3                  | 6-13                        | APEA *     |
| . Turkhanut<br>• • • • • • • • • • • • • • • • • • •        | ****             | (NCCPS)<br>ACCPS<br>(ACCPS)   |                        |                             | CUMULATIVE |
| 1000000<br>10000000<br>1000000                              | ***              |   |                        |                             | 3          |
| SCECO<br>SCECO  | ****             | (H)<br>(H)<br>(5.73)  | 1186<br>0.73           | 11 v. 0<br>(1.0.)<br>0 · 73 |            |
| 00000<br>00000<br>00000                                     | ***              | # 1 1 년 교 # 1 1 년 교 # 1 1 년 교 # 1 1 년 교 # 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | EAP STTS AGE (2.6-F)   | FE25 5726F                  |            |
| ert ent ert ent ent   | 0000             | S.UM<br>A.  | 1:1                    | 1714                        |            |



TIME IN HOUSS, AREA IN SQUARE MILES

|                                   | TIME OF HAX STAGE                               |               | 0.30      | 0.73      |
|-----------------------------------|---|---------------|-----------|-----------|
|                                   | MAXIMUM<br>STACE                                |               | 359.00    | 60.6      |
|                                   | BASIN   | 0.0           | 0.0       | 0.0       |
|                                   | TOW PERIOD 72-HOUR                              | 989.          | 1626.     | 1623.     |
| CHARL THEORE HE WANTE TO THE TIME | AVERAGE FLOW FOR MAXIMUM PERTON 22-HOUR 72-HOUR | 989.          | 1626.     | 1623.     |
|                                   | AVERAGE F                                       | 959           | 1626.     | 1623.     |
|                                   | T 120 10F                                       | C.07          | C.72      | C.73      |
|                                   | FLOR  | • 266         | 5632.     | 3237.     |
|                                   | STATION   | 41            | 24        | 24.3      |
|                                   | VOI 14 P 3 4 B                                  | HYDRCGRAPH AT | ROUTED TO | RCUTED TO |

|  | TIME OF<br>PAILURE<br>HOURS     | 0.28        |
|--|---------------------------------|-------------|
| 10P 0F 0AM<br>359.60<br>9371.          | TIME OF<br>MAX BUTFLOW<br>HOURS | 0.72        |
|  | DURATION<br>DVER TOP<br>HOURS   | 0.03        |
| SPILLEAY CREST<br>355,00<br>26.39      | MAX 1 PUN<br>CUTFLUM<br>CFS     | 3632.       |
| 14171AL VALUE<br>358.99<br>60.<br>980. | MAXIMUM<br>STOKAGE<br>AC-FI     | <b>60</b> • |
|  | NAXIVO<br>OVERPTHE<br>NAME      | 00.0        |
| FLEVATION<br>STURAGE<br>COTFLOR        | RESERVOIS<br>W.S.FLEV           | 359.00      |
|  | RATIO<br>CF<br>PHF              | 1.00        |
| P. LAN                                 |                                 |             |

ood NERMAL END OF JCB ood

| 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1 |      | PLATE LEKE GAM CYCKTOPPING ANALYSIS TO CONTY - NIA WARRING CONTY - NIA WARRING CONTY - NIA COLONIA - | 7LCH 1.0                              | INFLOW FEON SCS UNIT GRAPH COMPUTATIONS | 22.2<br>22.3<br>3.3 0.15 HG 112 123 1 | . 4         | 1 thy 100,1 x0 0 x23 0x x 103 110 133 | 155.1 191.1<br>106.1 191.1 | A3 ROUTE BUTFLOW HYDROGRAPH FROM BASS LAKE THROUGH I | STER - 1      | * 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 | A4 | 1 STCR -1 6000, 0.023 45 1 00 | 15. 10. 5. | AS ROUTE HYDRUGR | 0.1 0.05 0.1 10800. 0.008<br>0.1 12: 2459 250. 270. | AS DEVELOP LOCAL INFLOW HYDROGRAPH - BASS LAKE TO BLA | ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) |  |
|--|------|--|---------------------------------------|---|---------------------------------------|-------------|---------------------------------------|----------------------------|--|---------------|---|----|-------------------------------|------------|------------------|---|---|---|--|
|  | 9217 | P-4 p-4 P-4P   |                                       | The Store                               |                                       | ·           | e (), i                               |                            | <b>3</b> 62.5  | <u>. (a .</u> | u. 6.                                   | 1  | San Silve (in the             | . <b>ప</b> | <u> </u>         | _ CE se su Cs                                       | ¥€.3  | . (i i)                                 |  |
| e<br>Traditional res                     | ,    |  | • • • • • • • • • • • • • • • • • • • |   |                                       | :<br>!<br>! |                                       | !<br>!                     |  |               |   |    |                               |            | ا                |   |   |   |  |

| r. r |   |  |
|--|---|--|
| м <u>т</u> С-1 10FU1                     |   | 965.2 13345. 21421.<br>142. 1943. 2345.<br>365.2 368. 370.   |
| 3  | TO SLAIR LAKE                           |  |
| 100                                      | SAPES TO CAT TOTAL DIFLOW TO SLAIR LAKE | 78706548H THYRUGH FLAIS LAKE 357, 984, 2553, 4 357, 359, 361, 361, 1, 5  |
| ы С-1 тару                               | TEN DE SHOVE                            |  |
|  | egdack# Gylecoo                         | The state of the s |
| 171                                      | YY 17 C                                 | A SCHOOL AND A SCH |
|  | 4.67                                    | a a hie bie a.n.e.<br>a c. C. musioi azis a  |

|  | 1      |  | ,                                     |        |        |
|--|--------|--|---------------------------------------|--------|--------|
|  |        | ·  | }<br>                                 | ļ      | İ      |
|  | 1      | .  |                                       | }      | 1      |
| - 1  | 1      | į  | - 1                                   | 1      | - 1    |
|  | İ      |  |                                       |        | i      |
|  | •      |  |                                       | ì      | ļ      |
| -  | ł      | 1  | - 1                                   | i      |        |
|  | ļ      | İ  | - 1                                   |        | - 1    |
| ŀ  | -      | . !  | 1                                     | - 1    |        |
| - 1  | ·   -  | 1  | 1                                     |        | l<br>i |
| 1  |        |  | †                                     |        | ļ      |
| 1  |        | i  |                                       | Ī      |        |
| - 1  |        | 1  | - 1                                   | ļ      |        |
|  |        | -  | -                                     | İ      |        |
| 1  |        |  |                                       | 1      |        |
| i  |        | ļ  |                                       | ļ      |        |
|  | - 1    | i  |                                       | İ      |        |
|  |        | 1  | ļ                                     | į      | .!     |
|  | 1      |  |                                       |        | İ      |
| -  | - 1    | ļ  |                                       | ļ      | -      |
| į  | 1      | }  | !                                     | !<br>} | 1      |
| i  | ļ      | İ  |                                       | ĺ      | 1      |
| [  |        | [  | ĺ                                     |        | i      |
| ļ  | j      |  |                                       | ĺ      | 1      |
|  |        | ĺ  | i<br>:                                | ļ      | į      |
| 1  | !      | İ  | İ                                     |        | -      |
| ļ  | i      | ļ  | :                                     |        | ;      |
| !  | i      | į  | :                                     | !      |        |
| -  | 1      | į  | i                                     |        | b.     |
|  |        | :  |                                       | •      |        |
| į  | i      | :  |                                       | :      |        |
|  | *      |  | •                                     | •      | ,      |
|  |        |  |                                       |        |        |
|  | *      |  | :                                     |        |        |
|  |        | •  |                                       | !      |        |
| ĺ  | ٠      |  |                                       |        |        |
|  | :      |  | ٠                                     |        | :      |
|  |        |  | :                                     |        | ;      |
|  | :<br>• |  | :                                     |        | ;      |
|  | :<br>• |  | · · · · · · · · · · · · · · · · · · · |        |        |
|  | :<br>• | -  |                                       |        |        |
|  | :      | -  |                                       |        |        |
|  | :<br>• | -  |                                       |        |        |
| Charles of the state of the sta | :<br>• |  |                                       |        |        |
|  |        |  |                                       |        |        |
|  |        | The state of the s |                                       |        |        |
|  |        |  |                                       |        |        |
|  |        |  |                                       |        |        |
|  |        |  |                                       |        |        |
|  |        |  |                                       |        |        |
|  |        |  |                                       |        |        |
|  |        |  |                                       |        |        |
|  |        |  |                                       |        |        |
|  |        |  |                                       |        |        |
|  |        |  |                                       |        |        |
|  |        |  |                                       |        |        |
|  |        |  |                                       |        |        |
|  |        |  |                                       |        |        |
|  |        |  |                                       |        |        |
|  |        |  |                                       |        |        |
|  |        |  |                                       |        |        |
|  |        |  |                                       |        |        |
|  |        |  |                                       |        |        |
|  |        |  |                                       |        |        |
|  |        |  | -                                     |        |        |
| •  |        |  | -                                     |        |        |
| •  |        |  | -                                     |        |        |
|  |        |  |                                       |        |        |

| FLUID HYESTERAN, PARAGE (1003-  10. LATEOAZSZA1  11. LATEOAZSZA1  12. LATEOAZSZA1  13. LATEOAZSZA1  14. LATEOAZSZA1  15. LO  16. LO. 20  17. LATEOAZSZA1  17. LATEOAZSZA1  18. LO  18. LO  18. LO  19. LATEOAZSZA1 |
|--|
|--|

|   | 6014EN TIME 3.0  100  100  100  100  100  100  100   | 15781301100.  52.0 2.0 2.0 10.  1055         | 2.600 - 14111AP<br>2.100 - 14111AP<br>2.100 - 14111AP<br>2.100 - 14111AP<br>2.100 - 2.44<br>2.100  ### 12.0   123   123   123   123   123   123   123   123   123   123   123   133   1 |
|---|--|--|--|--|
| 1 000                                   | •  | AVERAGE                                      | 1 X A Y  | i<br>:   |
| 5. 709. 619<br>6. 777. 619<br>6. 8. 619 |  | -=   | 1-51/116W  | 4.7  |
| 2: 709: 619<br>6: 779: 619<br>6: 60     | ****   | **************************************       | **   |  |
| 2. 709. 619<br>6. 77. 600<br>0. 8. 600  |  | ا بن   | EA = 5.90  | \<br>\<br>   |
| 2. 709. 619<br>6. 777. 619              | _  | 5422(  | 5677   | 1  |
| 2. 709. 619<br>6. 77. 609               | 6  | UM AVERAGE                                   | X 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2  | •  |
| 2. 709. 619<br>6. 779. 619              |  |  | T STATION  | ( . 4 )<br>( . 4 )   |
|   | 645 INATES 752 752 109 12 109 109 109 109 109 109 109 109 109 109  | SS - PHY PHY PHY PHY PHY PHY PHY PHY PHY PHY | 2474<br>236<br>247<br>247<br>247<br>247<br>247   | 440  |
|   |  | 주 · · · · · · · · · · · · · · · · · · ·      |  |  |
|   |  | :  | TGRAPH   | Ü.   |
|   | The state of the s | 655<br>055 PATE<br>PPFRVIOUS ARE             | 4.15 US 14.1<br>1.15 US 14.16<br>1.16 PER 14.1   | i<br>H   |
|   | F  | 2.0 000 72 HR 1Ng                            | 0.041 0  | ~ UV   |
|   |  |  | HA PARCIPLIATA   |  |
| •                                       |  | FCIPITATION<br>IJJON ÇGEFFICIENT             | a coc H  | . S.   |
|   |  | ## OF-F                                      |  | STA  |

| 4 | 化光光 化光光 化化子 化化子 化化化 化化化 化化化 化化化 化化化 化化化 |
|---|---|
| •                                       | i<br>V                                  |
|   | ë<br>e<br>e                             |
|   | 6<br>6<br>8                             |
|   | *<br>&<br>&                             |
|   | 4<br>4<br>4                             |
|   | 4<br>4<br>4                             |
|   | <b>春</b><br>公<br>泰                      |
|   | ·<br>·<br>·                             |
|   | C<br>A<br>A                             |
|   | 수 수 ·                                   |
|   | 会<br>会<br>支                             |
|   | ë<br>e                                  |
|   | 후<br>경<br>유                             |
|   | 57<br>55<br>46<br>47                    |
|   | **<br>**<br>**                          |
|   | 수<br>수<br>수<br>수                        |
|   | 17                                      |
|   | 化 茶香香 经影响 医动物 人                         |
|   | (A) (A)                                 |
| ,                                       | V<br>V<br>V                             |
| •                                       | 会会会                                     |
|   | 春                                       |
|   | e<br>G                                  |
|   | 电电子 化聚化 电电路                             |
| ١                                       | e<br>e                                  |

| ST TO  | STEEP | 0, 0   VIII   VOI |             | 101.10 1.00 1.00 1.00 1.00 1.00 1.00 1. | PNTRCL AFR PLOT SCALE AFR PLOT SCALE CONSTRUCT SCALE 102.13 1 102. | 7100<br>61207<br>49.9<br>53.10<br>796.<br>03.10<br>***<br>***<br>1511:00 |                                | 84.6<br>105.10<br>2422.<br>105.10<br>3639.00<br>3639.00 | 102.0<br>106.10<br>3639.<br>106.10<br>119.00<br>5137.00 | 119.0<br>107.10<br>5137.<br>107.10<br>6921.00 | 137.6<br>108.10<br>6921<br>103.10<br>8777.60 | 154.0-105.10<br>3777. |
|--|---|---|-------------|---|--|--|--------------------------------|---|---|---|--|-----------------------|
| 101<br>10 13<br>11 10 101<br>11 10 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 101<br>11 1 | #40 #400<br>#40 #400  | (AC-FT)   | <b>u.</b> , | >-                                      | FAXIYUE AVESAGE  RAXIYUE AVESAGE  24-HE 24-HE 278-HE 154-70 154-70 164-70  |  | 65.09.<br>69.50-HF<br>79.50-HE |   |   |   |  |                       |

AD-A103 939

NEW JERSEY DEPT OF ENVIRONMENTAL PROTECTION TRENTON --ETC F/6 13/13

NATIONAL DAM SAFETY PROGRAM, BLAIR LAKE DAM (N-D07461-79-C-0011

UNCLASSIFIED

20 2

10 3

10 -81

10 -81

10 -81

10 -81

10 -81

10 -81

10 -81

10 -81

| <b>0</b>       |
|----------------|
| *              |
| ¢<br>¢         |
| è              |
| *              |
| #<br>#<br>#    |
| - 李春春          |
|                |
| 4<br>4<br>4    |
| ti<br>ti       |
| \$<br>\$<br>\$ |
| #<br>#<br>#    |
| *<br>***       |
|                |
| <del>Q</del>   |
| \$<br>\$<br>\$ |
| ě              |
| ÷              |
| **             |
| \$<br>\$<br>\$ |
| ***            |
| 4<br>4<br>4    |
| \$ 0.5<br>0.5  |
| \$<br>\$       |
| •              |
| *<br>*         |
| **             |
| *<br>*         |
| \$<br>\$<br>\$ |
| ***            |
| r<br>r         |
| ě              |
| ě.             |
| 40<br>40<br>40 |
| e<br>4         |
|                |
| *              |
| **             |
| *              |

1.000

|  |  |   |  | RIGHT DVERBANK<br>10.00<br>90.00 115.00  | 3.12 3.96 4.35                                      | 12629.64 14652.39 16904.67 | 13.42 14.21 15.00        | 0. TO 16905.   |  |   |   |                     |  |                     |
|--|--|---|--|--|---|----------------------------|--------------------------|--|--|---|---|---------------------|--|---------------------|
| GGRAPH FROM BASS LAKE THPOUGH REACH 1  |  |   | .ген сассисат10N   |  | 17FLBW CURYE 2.63<br>16 15.44 18.02                 | -0                         | 16 3.954.74-35-35-312.63 | DR GUTFLOWS BETWEEN  | ***  |   | 59.50-Ht<br>792.<br>20.687<br>6505.               | 99.50-HR            | 99.50-HE<br>1.49                               |                     |
| нуся                                   | PRINT CONTROL<br>PLUT CONTROL<br>HYCRGGRAPH PLOT SCALE | CR OF SUPERACHES OF INITIAL CCN01710N 13L COND 1710N NG - AND D COEFFICIENT | TING<br>LEFT OVERLANK N-VALUE<br>REIN CHAMMEL N-VALUE<br>REACH LENGTH<br>ENGRGY CLOPE<br>ENGRGY CLOPE<br>ENGRGY CLOPE<br>ENGRGY CLOPE  | 55-SECTION DATA CHANNEL 0.0 65.00 65.00 65.00  | 0.69 COMPUTED STORAGE CUTFLOW 2.25 9:10 10.90 13.44 | 7.95 6477.58 7744.44       | 3.16                     | OF LONSERICALLY UNSTABLE FOR OUTFLOWS BETWEEN OF LONSER PEACH LEWSTA | ***  | 1.00  | FINITION N  | 7. X                | MAX1408 AVEQACU 51AGE<br>54-88<br>5-55         | 12 08 06*           |
| 6 FOUTE BUTFLEW                        | ARTAPLES  1 0 1 0 ATE                                  | # 12 12 12 12 12 12 12 12 12 12 12 12 12                                    | L CEPTH CHANGL GOUTING ANCH CHANGE OF 100 HIEFT OF 100 HIEFT OF 1100 HIE | 15,46 16,26 25,00 25 | 0.0<br>6.03<br>7.45                                 | 5/11.6° 4426.11 5377       | 7.89 6.68                | TREATER WIFE   | 0.00   | - HYGAGAGARHAN STATION - FOR PLAN IN PATION | (CFS) 925743<br>(TUCHES) 14.5942<br>(EC-17) 45764 | 6-H3<br>15.         | 5-83<br>11.79                                  | CUPULATIVE ASEA = 5 |
| 00000000000000000000000000000000000000 | 23 KG GUTPUT   | 497475 STURY GR   | 1/W30k 33 52   | -27 fy FLEVATICH   | STORAGE   | <b>MOTULAS</b>             | - NOTHER PROPERTY        | AN LASA ING ABOUT DIFIED PUL.  | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ |   | 1000 FEON (HA)                                    | (20-FT) AGE (20-FT) | FEAST STAGE (FO)<br>(FEET) (FO)<br>15.14 (3.00 |                     |

|   | ****   | The state of the s | And the second s |         |
|---|--|--|--|---------|
| W W Y                                   | 0 44<br>**                                     | FOUTE HYDROGRAPH THROUGH SEACH 2   |  | •       |
| :                                       | ****   |  |  |         |
| a KC                                    | A LONG TOWN TOWN TOWN TOWN TOWN TOWN TOWN TOWN | of Variaties Paint Comfron 1 Plot Control 1 Plot Control Contr |  |         |
| LA. :                                   | DOLLOR<br>COMMON                               | FRANCI<br>CLUBCO<br>S Property<br>Clubco   |  |         |
| 3                                       | 40FFAL (FPT++)                                 | -CHANNEL-KUNTANG<br>3.100 LEFT DVENDANK N-VALUE<br>0.100 EIGHT CHERRY N-VALUE<br>0.0200 ENERGY ELOYE<br>0.0200 ENERGY ELOYE<br>0.0200 ENERGY ELOYE   | ULATICN  |         |
| >- %;<br>u/u/                           | DISTANCE :                                     | 15.00 10.00 49.90 50.00 65.00  | 5.00 FIGHT EVERBANK<br>5.00 10.00 15.00<br>65.10 90.00 115.00  |         |
| 1                                       | STORIGE 9.6-                                   | Computer STC 23.43 40.42   | 11.VE<br>20 9.85 11.69 14.34<br>.F5 66.35 76.71 87.92  | 103.60  |
| ;                                       | COTFLOW 1651:40                                | 4 5025.98 2489.88 2883.83 - 3841.26 - 4199.54  | -4942.19 -5775.09 6762.18  | 1335:53 |
| ELE                                     | ELEVATION C.G.                                 | a 6.79 1.58 2.37 3.16  | 11.84 12.63 13.42 14.21  | 15:03   |
| 2.48P.18.5                              | 77.  | TO RESIDE TO BE  | 115 BETHEEN 43. TO 7730.   |         |
| 1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 |  | PYCKUCKAPH AT STATION 44   |  |         |

|   |  | •  |   |             |  | vice or and because |  |  |                                    |   |                    |          | ericania Menuncia  |  |
|---|--|--|---|-------------|--|---------------------|--|--|------------------------------------|---|--------------------|----------|--|--|
|   |  |  | <b>3-384-488-438</b>                    |             |  |                     |  |  |                                    | 694.45                                      | 13492.73           | 15.60    |  |  |
| en commune companye . Server upo to a c   | ;<br>;                                 |  | ***                                     |             |  |                     |  |  | 000                                | 505<br>505<br>513                           | 11251.79           | 14.21    |  |  |
| Marian  | :                                      |  | *******                                 |             |  |                     |  |  | RIGHT NVERBANK 15.00 395.00 520.00 | 29.27                                       | 9277:91            | 13.42    | •  |  |
|   |  | The state of the s | - 0 00 0 - 000                          |             |  |                     | •  |  |                                    | 23.60                                       | 7554.29            | 12.63    |  |  |
| 2.50=118<br>783<br>20.685<br>6509.  | 99.50-HK<br>11.                        | 99.50-HR   | ***                                     |             |  | •                   |  | LEFT LVEPANK N-VALUE<br>NAIN CHAMSEL N-VALUE<br>RICHT LVERSANK N-VALUE<br>REACH LENGTH<br>PREACY SLUTH<br>PARS STORMS STORAGE ZOHTEL PH. CALCH ATTON   | 0 270.10                           | 04 CURVE<br>19.65<br>349.14                 | 6072.16            | 11.84    | *  | 99.50-HK<br>791.<br>20.681<br>6508.              |
| <b>.</b>  | \$10846F 99                            | 3.03<br>3.03   | ***                                     | . m         |  |                     | T10N<br>C1ENT  | IE   | DATA CHAINEL 0.0 276.00 276.00     | 282.13                                      | 303.34             | 3.16     | *  | :  |
| 2000<br>2000<br>2000<br>2000<br>2000<br>2000<br>2000<br>200   | AVERACE SIG                            | HR AVERACE 78-107  | ***                                     | ROUGH REACH | POL<br>OLOT-SCALE                        |                     | SUBREACHES<br>HITIAL CONDITION<br>MADITION<br>AND D CEFFICIENT   | NA VALUE<br>ANX NIVALUE<br>GGR-SIGRAD  | CTION DATA                         | COMPUTED STORAGE - CUTFLOW<br>222.84 282.13 | 3753.43            | 10.26    | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | AVERAGE 72-48<br>1099 -<br>20,611                |
| 20202.<br>203202.<br>636218.  | YAXIPUBA<br>ALHE                       | FAXIVE: 84-HK<br>8-07  | ***                                     | CGRAPH THR  | PRINT CONTR<br>PLET CONTRO<br>HYOREGRAPH |                     | NUMBER OF STATE OF THE CONTROL OF TH | 2007<br>1007<br>1007<br>1007<br>1007<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008<br>1008 | CEOSS-SECT<br>NK                   | 171.29                                      | 2665.67            | 1.50     | Jon<br>1 = 0   | 2007.<br>2007.<br>2007.<br>2007.<br>200.<br>200. |
| 16.20.00<br>16.20.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16.00.00<br>16. | 6- HR<br>11**                          | 16-HA<br>16-14   | ***                                     | POUTE HYDR  | RIABLES<br>1                             | DATA                | STUR<br>1.00<br>1.00<br>1.00   | 00.00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0  | FT NVERE                           | 3.92  | 34.22.<br>2198.98. | 9.79     | AT SIAT  | (-143<br>9070<br>14.299                          |
| (14-04)<br>(24-04)  |  | CURULATIVE   | ****                                    |             | TENTEDL VA                               | ROUTI               | TENSET INC.  | SEPTH CHAN   | 100                                | 91.31                                       | 1644.62            | 7.89     | AA<br>HYDSGGRAP  | (1200 CE S)<br>(200 CE S)<br>(300 CE S)          |
| 14.5.4<br>4.3.4.0   | 4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4. | 4 3.00   | ***                                     | 27          | CU TFUI                                  | UCF.                | 7. F. S. F.  | NGRKEL   | -ELEVATION-<br>PISTANCE            | TORAGE                                      | CUTFLOW            | £FVAT164 | ü  | 4 (0)  |
| 1000  | 16.25 CTT AGE<br>(20.277)              | 67.2 STAGE<br>67.2 STAGE<br>16.21  | *************************************** | . XX        | 35 KG                                    | •                   | 36-ks  | 37 RC  | 35 FX                              | S   | LO .               |          | \$\<br>\$\<br>\$\  | FEAN. ELGW<br>(CTS)<br>11597                     |

•

| 59.50-HK<br>99.50-HB   | s sate state | Z   | GIVEN TIME   | 4                                | 1 HYDPOGRAPH<br>643. 707. 671. 598. 566.<br>116. 91. 72. 56. 44. |
|--|--|---|--|----------------------------------|--|
| 1 24-HE AVERACE STORAGE<br>174.<br>XIMUR AVERACE STAGE<br>24-HR<br>27-50 22-HR<br>99 SC MI | NFL GH HYDROGRAPH - B  | IN AREA<br>L FLOW<br>GASE FLOW RECESSION  | PRECIPITATION CORPETCIENT   PRECIPITION CORPETCIENT   PROPETCIENT                             | 34 END HYD<br>34 ENC - OF - FER<br>167.                          |
| 7-48<br>494.<br>73-28<br>VE AFEA = 5.  | ore cro ore wee ere -<br>- DEVELUP-LOCAL-INFLO   | CTE   151105 SUPPAS<br>CTE   15105 SUPPAS<br>CTE   15105 SUPPAS<br>  15000 SECTION   15 | 5-10 Table  | TE 1.00 INTLES<br>6.15 UNITERAPH | 265.<br>232.<br>155<br>175<br>17                                 |
| TINE (HE) (HE) (HE) (HE) (HE) (HE) (HE) (HE  | 000 000 000 000<br>000000000<br>000000000<br>000000  | 01 24 2 10 0 4 4 5 4 6 4 6 6 4 6 6 6 6 6 6 6 6 6 6 6  | FRECIS IATION DA<br>FRECIS IATION DA<br>FRESSO<br>FRECEST OF I<br>FRECEST OF I   | UNIFCE LASS FA                   | 344.<br>375.<br>23.<br>23.                                       |
| ## STER AGE (12) ## ## ## ## ## ## ## ## ## ## ## ## ##                                    | 29 200 200 200 200 200 200 200 200 200 2   | 41 FA<br>42 EF  | 43-FK  | 0n 55                            |  |

|   |  |   |  |  | 1200.                                   |   |   | 7  | 000  |  |                                       | i i  | 1                                      |   |
|---|--|---|--|--|---|---|---|--|--|--|---------------------------------------|--|--|---|
|   |  | 1                                       |  |  | ļ                                       |   | Ì   | -  | *  |  |                                       | ₩<br>₩<br>₩  |  |   |
| <b>9</b> 765  | 0400   | - war                                   | ا<br>مىن رىن سىد   | ym ±w.                                       | nt-ma                                   | )<br>   | *D&C  | \$000<br>  | *  |  | 1                                     | 0  |  |   |
| <b>ゆらら</b> る  | 7777   | ーーーーー                                   | - r-33 a :   | ひにかない  | 1. いひょえい                                | アコリワ  |   |  | ř  |  |                                       | #  |  |   |
| !.<br>ခရုပ္ရေ   | ( C C C C C C C C C C C C C C C C C C C  | ၂<br>၂                                  | ပစ္စစ္သာက<br>၂   | )<br>1020'                                   | )<br> <br>                              | )<br> <br>  | <br>  | )<br>500   | k<br>*   |  |                                       | #<br>#   |  |   |
| きじこう  | ほうじょう  | 24                                      | レート:   | 1.000  | 10000<br>10000<br>10000                 | 10" "   |   | Acres  | 6  |  | 1                                     | #<br>#   |  |   |
|   |  |   |  | Ì  |   |   |   |  | *  |  | }                                     | 45   | Ì                                      |   |
|   |  |   | ]  | ļ  |   |   | }   |  | <b>\$</b>  |  |                                       | *  |  |   |
| 4444  | 2444   | \$ 44 4.<br>                            | ****   | 1444.<br>                                    | ***                                     | 440   | <br> <br>  Teneral Penetra | יטיטיטי  | *  |  |                                       | *  |  |   |
| l<br>market   | ****   |   |  |  | <u> </u><br>                            |   | l<br>Lace de de   | <u> </u>   |  |  |                                       | 4  |  |   |
|   |  |   |  |  |   | ү яги и<br>   | ****  |  | *  |  |                                       | *  |  |   |
|   | ין<br>ישישופים:  | ា<br>មាលាសាធារ                          |  |  |   | ນໜານ<br>  |   |  | \$<br>\$   |  |                                       | *  |  |   |
| س سست   |  |   |  |  |   |   |   |  | *  |  |                                       | *  |  |   |
| ;   |  | -                                       |  | 1  | -                                       | İ   |   | 1.   | \$<br>\$   |  |                                       | **************************************   |  |   |
|   | 1  | ;                                       | ļ  | !  | 1                                       | 1   |   | 1  | \$<br>\$   |  |                                       | ₽<br>₽   | l w                                    |   |
| 9786  | こところ   | こころく                                    | くらうろこ  | יטונטעוע                                     | <i>ነ</i> ን የሰነም የጉ                      | ***   | とせせせ  | 440  | `&<br>&  |  | i                                     | 1 **   | ¥                                      |   |
|   | •  |   |  |  |   | :   |   | İ  | \$ .   |  | İ                                     | **   | الا<br>ال                              |   |
| \$000<br>\$000<br>\$000   | 0 500<br>monst<br>manne  | 3000<br>11000<br>11000                  | これのできる   | 10000<br>10000<br>10000                      | 50000<br>50000<br>50000                 | 2000<br>2000<br>2000  | 0000<br>5000<br>5000  | 000<br>nom   | *<br>*   | •  |                                       |  | LAI                                    |   |
|   |  |   |  |  |   |   |   | 000  | \$ TX  | いらら  | :                                     | : 🔅  | <b>1</b> 8 0                           |   |
|   |  |   | ;  |  | :                                       | :   | ·   | i  | ቅ .<br>ው   | 20.  | :                                     | 장<br>상<br>45   | . [                                    | نب<br><u>ئ</u> ا  |
| usqusq  | אנט נגזינט נגא   | <b>ጥ</b> የነጣጥ:                          | <b>ጥ ሮክ</b> ማለነ (  | ብጣጠጠ   | <sub>ው</sub> የገለባ የጎ                    | กูลเกต  | ಗ, ಆತ ಆ   | ;<br>\$3\$   | 66   |  | :                                     | ů<br>ů   | č                                      |   |
|   |  |   | ·<br>•   |  | :                                       | i   |   | ,  | &<br>&   |  |                                       | , <b>#</b>   | 1911                                   | 14 00<br>00 00 00 00 00 00 00 00 00 00 00 00                                  |
| ***   | ***  | 4040                                    | ***  | ****   | ទទទទ                                    | * * * *   | ***   | 计分分类   | 후<br>참<br>참 보고 :   | •••  | ,                                     | <b>☆</b><br>☆<br>☆   | ر.                                     | 9   |
|   |  |   |  |  |   |   |   |  |  |  |                                       |  | 7.                                     |   |
|   |  |   |  |  | • • • •                                 |   |   | 1  | 4 U.O.   | 15-CJ  |                                       | . <u>e</u>   | JT A                                   | Ϋ́  |
| よりむく  | 100 C  | チェラー                                    | つくひるしょう  | げてこの   | しゃくいこってい                                | <b>してら</b> び  | 0000  | 20.5   | ######################################                       | 15-CJ  |                                       | 45   | 101                                    | HdV   |
| よりむく  | 1014444<br>10161011111111111111111111111111  | うとりきょう                                  | アクしょう  | ひこうじょうてき                                     | しゃくいこってい                                | じじゅう  | ら <b>しまっ</b>  | #222<br>#222<br>#222<br>#324<br>#344   | ## 122   | 55.2   |                                       | **   | = 5                                    | CRAPH   |
| よりむく  | ここ でいいうしょ  | うとりきょう                                  | アクしょう  | ひこうじょうてき                                     | これりょう                                   | じじゅう  | ら <b>しまっ</b>  | #222<br>#222<br>#222<br>#324<br>#344   | VERAGE PL  | 55.2   | · · · · · · · · · · · · · · · · · · · | **   | 0 GET TOT                              | DFUCKAPH  |
| ・<br>・<br>・<br>・<br>・<br>・<br>・<br>・<br>・<br>・<br>・<br>・<br>・<br>・  | <ul><li>ウェベル</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン</li><li>ロークラン<td>4 men</td><td>1 0 0</td><td>で<br/></td><td>6 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2</td><td>2426<br/>1 404<br/>1 404<br/>1 404<br/>1 404<br/>1 404</td><td>2276<br/>2276<br/>2136<br/>2136</td><td>6-1402<br/>1121<br/>0 698</td><td>AVERAGE FL</td><td>20 3<br/>552 5<br/>0</td><td>· In-0!</td><td>***</td><td>S TO GET TOT</td><td>HYDFOCKAPH</td></li></ul> | 4 men                                   | 1 0 0  | で<br>  | 6 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | 2426<br>1 404<br>1 404<br>1 404<br>1 404<br>1 404   | 2276<br>2276<br>2136<br>2136  | 6-1402<br>1121<br>0 698  | AVERAGE FL   | 20 3<br>552 5<br>0                                       | · In-0!                               | ***  | S TO GET TOT                           | HYDFOCKAPH  |
| イトミシ<br>・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・  | 101 (4 (4 (4)<br>101 (4 (4) (4)  | 4 men                                   | 1 0 0  | で<br>  | 6 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | 2426<br>1 404<br>1 404<br>1 404<br>1 404<br>1 404   | 2276<br>2276<br>2136<br>2136  | 98   | INUN AVERAGE FL  | 5410. 20.7<br>5410. 5552                                 | - 50-                                 | **   | APHS TO GET TOT                        | YDFOCKAPH   |
| \$0000<br>\$0000<br>\$0000  | 00000000000000000000000000000000000000   | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0   | \$0000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000<br>\$2000 |  |   | 00 00 00 00 00 00 00 00 00 00 00 00 00  | 0-0   | 99-1402.<br>0 100 E98.   | ANTWON AVERAGE FL  | 20.7<br>410. 552   | · 60- 56-                             | ***  | GRAPHS TO GET TOT                      | CR CF HYDROCKAPH  |
| 0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0. | 170<br>170<br>170<br>170<br>170<br>170<br>170<br>170<br>170<br>170   | 10000000000000000000000000000000000000  | 2000<br>2000<br>2000<br>2000<br>2000<br>2000<br>2000<br>200  |  | 10000000000000000000000000000000000000  | 1000<br>1000<br>1000<br>1000<br>1000<br>1000<br>1000<br>100   | 276<br>276<br>276<br>276<br>276<br>276<br>276<br>276<br>276<br>276  | 030 98 1402.<br>100 99 1121.<br>130 100 895.   | MAXIMUN AVERAGE FL   | 5410. 20.7<br>5410. 5552                                 | co sa-                                | ***  | OPCCRAPHS TO GET TOT                   | AZK GF HYDROGKAPH   |
| 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000  | 00000000000000000000000000000000000000   | 10000000000000000000000000000000000000  | 2000<br>2000<br>2000<br>2000<br>2000<br>2000<br>2000<br>200  |  | 10000000000000000000000000000000000000  | 1000<br>1000<br>1000<br>1000<br>1000<br>1000<br>1000<br>100   | 276<br>276<br>276<br>276<br>276<br>276<br>276<br>276<br>276<br>276  | 0100 99 1821.<br>0130 100 898 1821.  | MAXIMUN AVERAGE FL   | 3 20-288 20-39<br>5410- 5528                             | · 60- 56-                             | ***************************************  | CGRAPHS TO GET TOT                     | CR CF HYDROCKAPH  |
| # 030<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1  | 00000000000000000000000000000000000000   | 20000000000000000000000000000000000000  | ######################################   | STORMS OODS OODS OODS OODS OODS OODS OODS OO | 10000000000000000000000000000000000000  | 7.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000  | 2360 955 276 276 276 276 276 276 276 276 276 276  | 0100 99 1121.<br>0100 100 ESS.   | MAXIMUN AVERAGE FL   | 733 26-288 20.49<br>42. 5410. 552                        | A-=5,00-50-                           | 00 404 000 000 000 000 000   | ME HYDPECRAPHS TO GET TOT              | M NUPRIER OF HYDEOCKAPH   |
| # 030<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1000<br># 1  | 00000000000000000000000000000000000000   | 20000000000000000000000000000000000000  | ######################################   | STORMS OODS OODS OODS OODS OODS OODS OODS OO | 10000000000000000000000000000000000000  | 7.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000  | 2360 955 276 276 276 276 276 276 276 276 276 276  | 3 0100 99 1121.<br>3 0100 99 1821.<br>3 0130 100 895.  | 6-17 AAX TAUN AVERAGE FL                                     | 2942. 20.75<br>2942. 5410. 5527                          | 9t/=5,60-50-                          | 44 444 444 444 444 444 444 444 444 444   | ME HYDPECRAPHS TO GET TOT              | TION AUPROR OF HYDROGRAPH   |
| 40000000000000000000000000000000000000  | 20000000000000000000000000000000000000   | 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 20000000000000000000000000000000000000   | TO TO TO TO TO TO TO TO TO TO TO TO TO T     | 10000000000000000000000000000000000000  |   | 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2   | 3 0100 99 1121.<br>3 0110 69 1121.   | MAXIMUN AVERAGE FL   | 2942. 20.75<br>2942. 5410. 5527                          | € 42€ A-=5 , 60 5q-                   | 00 000 000 000 000 000 000 000 000 000   | HYDFCGRAPHS TO GET TOT                 | INATION - NUMBER OF HYDROCKAPH  |
| 10000000000000000000000000000000000000  | 00000000000000000000000000000000000000   | 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 20000000000000000000000000000000000000   | TO TO TO TO TO TO TO TO TO TO TO TO TO T     | 10000000000000000000000000000000000000  |   | 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2   | 3 0100 99 1121.<br>3 0110 69 1121.   | ACCOMPANA MAXIMUN AVERAGE FL                                 | 14,733 26,288 20,7<br>5410, 555,7                        | IVF- 42EA-=5, CO- SQ-                 | d can pro year one ben con add do  | CHAIRL HYDECGRAPHS TO GET TOT          | INATION - NUMBER OF HYDROCKAPH  |
| 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4   | 2000<br>2000<br>2000<br>2000<br>2000<br>2000<br>2000<br>200  | 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4   | 20000000000000000000000000000000000000   | ######################################       | 10000000000000000000000000000000000000  | 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4   | 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2   |  | AAXIVON AVERAGE FL.  | 5) 14.753 20.788 20.77                                   | IVF- 42EA-=5, CO- SQ-                 | 000 000 000 000 000 000 000 000 000  | CHAIRL HYDECGRAPHS TO GET TOT          | COMPINATION 2 NUMBER OF HYDRUCKAPH  |
| 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4   | 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2  | 20000000000000000000000000000000000000  | 20000000000000000000000000000000000000   |  | 10000000000000000000000000000000000000  | 700 00 00 00 00 00 00 00 00 00 00 00 00   | 2   | 4. 8 3 0100 99 1121.<br>6. 8 3 0100 99 1821.<br>7. 8 8 9 0130 100 898.                         | Acceptation of the Max I will average FL 6-42 6-42 6-42 7233 | 14-733 26-786 20-7<br>20-77 5410. 5527                   | IVF- 42EA-=5, CO- SQ-                 | s end not the test that the state and the test t | CERRICL HYDREGRAPHS TO GET TOT         | J COMPINATIONS AUPRER OF HYDROCKAPH   |
| 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4   | 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2  | 20000000000000000000000000000000000000  | 20000000000000000000000000000000000000   |  | 10000000000000000000000000000000000000  | 700 00 00 00 00 00 00 00 00 00 00 00 00   | 2   | 34. 8 3 0100 99 1121.  | ######################################                       | CHEST 14.733 26.788 20.77<br>C-FT 2942. 5410. 5557       | γε. 45£ Α-=5,60-5Q-                   | o de de de de de de de de de de de de de   | COMBINE HYDECORAPHS TO GET TOT         | OGGO<br>BARN COMPINATION<br>ICCMP   |
| 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4   | 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2  | 20000000000000000000000000000000000000  | 20000000000000000000000000000000000000   |  | 10000000000000000000000000000000000000  | 700 00 00 00 00 00 00 00 00 00 00 00 00   | 2   | 34. 8 3 0100 99 1121.  | 60000000000000000000000000000000000000                       | 18 (30-77) 14-733 26-788 20-77 (30-77) 5527              | IVF- 42EA-=5, CO- SQ-                 | 400 404 000 404 404 404 400 400 400 400  | L7 0 CENSING HYDFEGRAPHS TO GET TOT    | ersoco<br>Storiph Commination<br>Itone Ge Hydedoraph                          |
| 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4   | 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2  |   | To C C C C C C C C C C C C C C C C C C C   | 2000   | 1                                       | 193. 8 193. 8 193. 193. 193. 193. 193. 193. 193. 193.   | 2 230 95 276 276 276 276 276 276 276 276 276 276  | 45 35. 8 3 0100 99 1121.<br>50 30. 8 3 0130 100 898.   | ######################################                       | (1) CRES 14.733 26.288 20.7 (a.c.+FT) 2942. 5527         | IVF- 42EA-=5, CO- SQ-                 | 44 444 400 444 444 444 444 444 444 444   | CDMBINE HYDREGRAPHS TO GET TOT         | ooorrooo<br>HYGSEGEARH COMPINATION<br>1 NUMBER OF HYDRUGKAPH                  |
| 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4   | 20000000000000000000000000000000000000   |   | To C C C C C C C C C C C C C C C C C C C   | 2000   | 1                                       | 193. 8 193. 8 193. 193. 193. 193. 193. 193. 193. 193.   | 2 230 95 276 276 276 276 276 276 276 276 276 276  | 45 34 8 3 0100 99 1121.<br>50 30. 8 3 0100 99 1121.  |  | (10 CHES) 14.733 26.280 20.7<br>(ac-f1) 2942. 5410. 5552 | IVF- 42EA-=5, CO- SQ-                 | \$\$\$ \$\$\$ \$\$\$ \$\$\$ \$\$\$ \$\$\$ \$\$\$ \$\$\$ \$\$\$ \$\$  | ACCOCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC | AYUSTGEZARM COMPINATION<br>1 YUSTGEZARM COMPINATION<br>2 NUMBER SE HYDRUCKAPH |
| 2000 000 000 000 000 000 000 000 000 00   | 20 - 20 - 10 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -   | 20000000000000000000000000000000000000  | 20000000000000000000000000000000000000   |  | 10000000000000000000000000000000000000  | 100 - | 2 230 95 230 95 230 230 85 250 85 250      | 50. 45 54 8 3 0100 98 1121.  | TIME MAXIMUM AVERAGE FL  (HS)                                | (10 CHES) 14.733 26.280 20.7<br>(ac-f1) 2942. 5410. 5552 | IVF- 42EA-=5, CO- SQ-                 | 44 444 400 444 444 444 444 444 444 444   | CDMBINE HYDREGRAPHS TO GET TOT         | saabaassaabaabaa<br>HYGSEGBARH CAMAINATIDN<br>2 NUMMER GE HYDRUGSAPH          |
| 2000 000 000 000 000 000 000 000 000 00   | 21   |   |  |  | 100000                                  | 7.00 41 193 8 193 8 19 19 19 19 19 19 19 19 19 19 19 19 19  | 200 46  | 2335 - 68 34 8 3 0100 99 1121.<br>6055 45 35 8 3 0100 99 1121.<br>6035 56 30 8 3 0130 100 895. | # TIME   | (10 CHES) 14.733 26.280 20.7<br>(ac-f1) 2942. 5410. 5552 | IVF- 42EA-=5, CO- SQ-                 |  | COMBINE HYDROGRAPHS TO GET TOT         | saabaassaabaabaa<br>HYGSEGBARH CAMAINATIDN<br>2 NUMMER GE HYDRUGSAPH          |
| 2000 000 000 000 000 000 000 000 000 00   | 200  |   |  |  | 100000                                  | 7.00 41 193 8 193 8 19 19 19 19 19 19 19 19 19 19 19 19 19  | 200 46  | 2357 - 48 - 34 - 8 - 3 0100 98 - 1402. 0030 56 0100 98 - 1402. 0030 56 030 50 0100 698.        | Ch   | (1) CHES 14.733 20.788 20.77<br>(AC-FT) 2942. 5410. 5527 | IVF- 42EA-=5, CO- SQ-                 | \$40 \$40 \$40 \$40 \$40 \$60 \$60 \$60 \$60 \$60 \$60 \$60 \$60 \$60 \$6  | CONDING HYDECORAPHS TO GET TOT         | **************************************  |
| 2000 000 000 000 000 000 000 000 000 00   | 200  |   |  |  | 10000000000000000000000000000000000000  | 7.00 41 193 8 193 8 19 19 19 19 19 19 19 19 19 19 19 19 19  | 2350 46   | 1. 2352. 48 33. 8 3 0100 99 1121. 2 0550 50 50 1121.   | Ch TIME  | (10 CHES) 14.733 26.280 20.7<br>(AC-FT) 2942. 5410. 5527 | IVF- 42EA-=5, CO- SQ-                 | 44 444 448 444 448 444 484 484 484 484   | COMBINE HYDROGRAPHS TO GET TOT         | saabaassaabaabaa<br>HYGSEGBARH CAMAINATIDN<br>2 NUMMER GE HYDRUGSAPH          |

ecoposita per esta contrata de proposita de

HYDGGGRAPH AT STATTER SUR OF 2 HYDE GRAPHS PLAN 1, GALIG = 1,00

|   |  |  |                        |   |  | •  |  |  | •                                     |                                       |                       |
|---|--|--|------------------------|---|--|--|--|--|---------------------------------------|---------------------------------------|-----------------------|
| †<br>1<br>1                             |  |  |                        |   |  | •  |  |  | :                                     | * * * * * * * * * * * * * * * * * * * | !                     |
| 360 000 000                             | 0 000 000 000 000 000  | * 444  | ***                    | * ***   | ***                                      | *****  | 000 000 00                                   | ***  | ***                                   | ***                                   | ****                  |
| 4E KK                                   | 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4  | ROUTE INF  | LCW HYDRG              | GRAPH T   | HROUGH BLAIR                             | LAKE   |  |  |                                       |                                       |                       |
| 46-6.5                                  | HYSECCEAPH ECUT  | 1:5 DATA #9 STOR   | : ! iiU                | SUSTENCE ACHES TO CONTROL   | : <u>⊢</u>                               |  |  |  |                                       |                                       |                       |
| AS 73                                   | ' (  | 0.0  | 24.0                   | 30 - 30 ·   | FICIENT                                  | 0.09   | 80.0   | 109.0  | 142.0                                 | 193.0                                 | 235.0                 |
| 53.08                                   | CLEVATION  | 340.70   | 355.00                 | 356.00  | 357.00                                   | 359,00   | 361.00                                       | 363.00   | 365.20                                | 368.00                                | 376.00                |
|   | 394713513  |  |                        | 123   | 34н.                                     | 984.   | -2253  | 4122.  | 6746.                                 | 13345*                                | -2142 <del>1.</del> - |
| 51 55                                   | £LEVATIED  | 340.70   | 355.00                 | 356.00  | 357.00                                   | 359.00   | 361.00                                       | 363.00   | 365.20                                | 368,00                                | 370.00                |
| 5                                       | 6. SUN   | 6.4<br>6.4<br>6.5<br>6.5<br>6.5<br>6.5<br>6.5<br>6.5<br>6.5<br>6.5<br>6.5<br>6.5   | SPILLERAY<br>FEDICESAN | CREST ELEV<br>FICTENT<br>GREAT  | ELEVATION<br>D                           |  |  |  |                                       |                                       |                       |
| -55-55                                  | ALCONOMICS AND CONTROL OF THE CONTRO | 33.00<br>9.30.00<br>9.30.00  | EXECUTE                | FICIENT   | ОАМ                                      |  |  |  |                                       |                                       |                       |
|   | STORAGE 0.0  | 9.7  | 30.06                  | PUTED<br>40.0   | *** '<br>STGRAGE-CUTFLOW                 | LOW CURVE  | 109.00                                       | 142.00   | 193.00                                | 235.00                                |                       |
| 100000000000000000000000000000000000000 |  | 0.0  | 123.00                 |   | 964,00                                   | 348.00 964.00 2253.00 - 4122.006748.0<br>sesses ses ses ses se se se se se se se | - 4122.00                                    | 6748+00  | 13345+09                              | -21421-6                              | 0                     |
|   |  |  |                        | FLAN 1,   | AT STATIC                                | 1.00 AB  |  |  |                                       |                                       |                       |
| # 0000000                               |  | TO THE STATE OF TH |                        | 6 6 40004C<br>5 9 40004C<br>6 8 600000C<br>6 8 600000C<br>6 8 600000C<br>6 8 60000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 8 6000C<br>6 | 0001FLD8<br>3365<br>4356<br>4556<br>4556 | 0.0 4 6 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0                                    | 71 A G H W W W W W W W W W W W W W W W W W W | MON HRPH OFO CUTFLCW STGFLCE 1930 135 31 25 25 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 | 080 CUTFL<br>135<br>137<br>140<br>140 | CW STOP LCE                           | o mamman              |

| ക്രീക്കയ് സ്വയ്യൻ ഇന്ന് സ്വാഹിന് സ്വാഹി നായ് നിയാണ് നിയില് പിയാന് നിയിലായില് വാധ്യാവയില് സ്വാഹിയില് നിയിസ് വാധ<br>ഇത് ഇത് ഇത് ഇത് ഇത് ഇത് ആന് ഇത് ഇത് ഇത് ഇത് ഇത് ആന് വിവാധി നിയില് പ്രവേശില് എൽ ആദ്യ ആന് എന്ന് ഉത്വാന് വിവാഹിയി   | Nation &  |
|--|---|
|  |   |
| ം ഇത് ഇത് അത്രീക്ക് തിരുന്നത്ത്രത്തെന്ന് വേധിന്റെ വരുന്നത്ത് വാത്രവുന്നു. ഇത് വേശിക്ക് വരുന്നത്ത് വരുന്നത്ത് ആ<br>ഇത് അടിയ്ക്ക് സ്വിധ്യാന് നിരുന്ന് സ്വിധയിൽ നിയ്യി വരുന്നത്ത് നിയ്യില് വരുന്നത്ത് വരുന്നത്ത് വരുന്നത്ത് വരുന്ന  | ທານ ອ   |
| ณณฑตรมกระทางเขาการความหาการความหาการความหาการความหาการความหาการความหาการความหาการความหาการการความหาก<br>   | · · · · · · · · · · · · · · · · · · ·   |
|  | *   |
| יים אין אין אין אין אין אין אין אין אין אין  |   |
|  | *   |
|  | ě.  |
| とりをもとしているとうできまってものようでもというというからものとうももとうものもれるものものものものものののののののののとうないというというというというというというというというというというというというという   | ೦೦೦ 💠   |
| and properties and and and and and appear and meaning and and and and and and and and and and  | ⊸⊶r. §  |
| COCOC CANNINANNAL THE THE THE THE THE TOCOC COCOC COCOCOCOCOCOCOCOCOCOCOCOCOC  | ∠num ≥  |
|  |   |
|  | Š   |
|  | ∻   |
| ファイト ちょうしゅうしょうしょうしゅう とうしょう とうしょう とうしょう ちょうしょう ちょうしょうしょう ちょうしょ しょうしょ しょうしょ しょうしょう しょうしょ しゅうしょ しゅうしょ しゅうしゅう かんかん かかかん かんかん かかかん かんかん かんかん かんかん かん  | *   |
| TO THE TOTAL STATE TO THE STATE TO THE TOTAL STATE OF THE CORCE TO THE TOTAL STATE OF THE | ನಾನಾನಾಗು ಕ  |
| ૽૿ૹ૽૽ઌ૽૽ઌ૽ૺઌ૽૽ઌ૽ઌ૽૽ઌ૽ઌઌઌઌૻઌૻઌૻઌઌઌ૽ઌૻૡૻઌઌઌઌઌઌઌ૽૽ઌઌ૽ઌઌઌઌઌઌઌઌ   |   |
| およみてようとはりまるりまちょうこのでしょうのうとうのうとうのうとようできょうりょうできょうという。   |   |
| ごうりょう ウップラウムエム ちゅうてん サールキャ ゴンドライク ゴウ ちょうり とちゅう クラー・とう ちゅうしょう ファンファンファン マンドラ てんしょう ヤッション マーク マール・エー・スティー・スティー・スティー・スティー・スティー・スティー・スティー・スティ  | ಎಂಬಂದ 🧇   |
| mander on Color Color Color Color on the color of the col | 9<br>9<br>4   |
|  | 4<br>4  |
| HÍ DHÁ Á HÁ MI MÁ GÁ MÁIL BORHÁO RIOMRAÍONAÍ Ó RAÍ RAÍ RAÍ RAÍ RÓ FHÁ GÉ FHÁ CHA CHAIR<br>HA CHAIR THE FÍOLAGAIC A RAÍ MHÉIMHAIN ME A HA CHAIR MEARACHTHA A CHAIR A GE THA GÉ FHÉIR A GA CHAIR<br>HA CHAIR GHA CHOIR GA RIOMRAÍON A BHORNAGH THA HA CHAIR A RAINN ROCHA GÉ FHÉIR A GA CHAIR A GA CHAIR A GA CHAIR  |   |
| THE TOTAL OF THE COLUMN TOTAL OF THE TOTAL OF THE THE THE THE TOTAL OF THE THE THE THE THE THE THE THE THE THE   | )<br>E  |
|  | · ·   |
|  | in the state of   |
| COUNTY STANDED SENDING SENDING SENDING SENDING SENDING SENDING COOLOO SENDING  |   |
| PREPARAMENTAL CONTRACTOR OF COLOR OF THE PROPERTY OF THE PROPE |   |
|  |   |
| PREPARAMENTAL CONTRACTOR OF COLOR OF THE PROPERTY OF THE PROPE |   |
| PREPARAMENTAL CONTRACTOR OF COLOR OF THE PROPERTY OF THE PROPE | 17.00<br>17.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00 |
|  | 1000 1000 1000 1000 1000 1000 1000 100  |
| es e o es e es e e e e e e e e e e e e e   |   |
| A SA SA SA SA SA SA SA SA SA SA SA SA SA   | 100.1 100.0 114.0   |
| es e o es e es e e e e e e e e e e e e e   | 100.1 100.0 114.0   |
|  | .1 17.00 17.4.20 17.7.00 17.7.  |
|  | 7.0 20.05.7 6 5 17.00 18  |
|  | 7.0 20.05.7 6 5 17.00 18  |
| ETHER BUT AND THE TOTATE TO A SOCIETATE THE TOTAL TO THE TOTAL THE | 1. 57.0 U.S. F & 3 1.700 IGG  |
| antiphinonenty and another control of the control o | 1. 57.0 U.S. F & 3 1.700 IGG  |
| THE CONTROL OF SECTION OF THE CONTROL OF SECTION OF THE CONTROL OF SECTION OF THE CONTROL OF THE | 1. 57.0 U.S. F & 3 1.700 IGG  |
| SE SHILMAR AND SE SHILMARAN SECHIMARAN PERSONAN AND PERSONAN AR SINS COMMON SECHIMAR SECHIMARAN AND SECHIMARAN PERSONAN AR SINS COMMON SECHIMARAN SECHIMAR | 4 (1. (2.1) (2.1) (3.1)   |
| Signature in the Centralition of the Centralit | 54 51 57.0 305.7 6 3 17.00 18.00 6 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6  |
| See Service and a consideration of the construction of the constru | 250 64 61 270 12<br>250 65 170 12<br>250 67 170 12<br>250 67 170 120 120 170 6 3<br>250 67 170 120 120 170 6 3<br>250 67 170 120 120 170 6 3<br>250 67 170 6 3  |
| 25 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2   | 250 64 61 270 12<br>250 65 170 12<br>250 67 170 12<br>250 67 170 120 120 170 6 3<br>250 67 170 120 120 170 6 3<br>250 67 170 120 120 170 6 3<br>250 67 170 6 3  |
| See Service and a consideration of the construction of the constru | 250 64 61 270 12<br>250 65 170 12<br>250 67 170 12<br>250 67 170 120 120 170 6 3<br>250 67 170 120 120 170 6 3<br>250 67 170 120 120 170 6 3<br>250 67 170 6 3  |

pasasasasasas as a constant of the constant of PRESENT AT TIME 43, 50 BIRDER AN CUTHICH IN

|               |   |   |  |             |        |   | *************************************** |   |          |          |        |   |        |          |
|---------------|---|---|--|-------------|--------|---|---|---|----------|----------|--------|---|--------|----------|
|               |   |   |  |             |        |   | '                                       |   | 1        |          |        |   |        |          |
|               |   |   |  |             | ,      |   |   |   |          |          | •      |   |        |          |
|               | i<br>I  |   |  | Ì           | İ      |   |   |   |          |          |        |   |        |          |
|               |   |   |  |             | ĺ      |   |   |   |          |          | !<br>! |   |        |          |
|               |   |   |  |             |        |   |   |   | [        |          |        | • |        |          |
|               | ·   ·   |   | 1  | 1           |        |   | [                                       |   |          |          |        |   |        |          |
| 1             | · [   |   |  |             |        |   |   |   |          |          |        |   |        |          |
|               | :   | j   |  |             |        |   |   | Ì |          |          |        |   |        |          |
|               | Ţ   |   |  |             |        |   |   | į | 1        |          |        |   |        |          |
|               | 1.  | Ì   |  | Ì           |        |   | }                                       |   |          | <u> </u> |        | ) |        |          |
|               |   |   |  |             |        |   | İ                                       |   |          |          | İ      | ł |        | •        |
|               |   |   |  | j           | j      |   |   |   |          |          |        |   |        |          |
|               |   |   |  |             |        |   |   |   |          |          |        |   |        |          |
|               |   |   |  |             |        |   |   |   |          | 1        |        |   |        |          |
|               | :   |   |  |             |        |   |   |   | İ        |          |        | İ |        |          |
|               |   |   |  | ;<br>1      | j      | 1 | }<br>]                                  |   |          |          | !      |   |        |          |
|               | :   | •   | !  |             |        | 1 |   |   |          |          | İ      |   | !<br>] |          |
|               | ,   | !   | !  |             |        |   |   |   |          | •        |        |   |        |          |
| ,             | ₹.<br>50.<br>•                                      | ± •   | <b></b> 40                               | :           | !      |   |   |   | :        | i<br>L   | ì      | i |        |          |
|               | 7.50-HE<br>1467.<br>20.750<br>12000.                | 7.3   | 27.                                      |             |        | ! | [                                       |   |          |          | 1      | : |        |          |
|               | 90.<br>22.<br>12.                                   | 4H-05.65                                      | 99.59-HE<br>357.02                       | :           |        | l | !                                       |   | :        | •        | :      |   | :      | !        |
|               | ů,  | Ú,  | , c                                      |             |        |   |   |   |          |          | •      |   |        |          |
|               |   | £ 5   | Ш  |             | i<br>i |   | ;<br>!                                  | • | }        | !        | •      | : | i      | !        |
|               | 2 PEGE<br>2019<br>2005<br>12011                     | \$106.46F<br>72-HP                            | 47FRAGE 72-HF                            |             | • •    |   |   |   |          |          | 1      |   | :      | 1        |
|               | E 500 - 0   | 227   | 25.25                                    | :           | 1      |   | !                                       | i | , -      | 1        |        |   | •      | ;        |
|               | AVERAGE   | ئ   | . A 6.                                   | :           |        |   | 1                                       |   |          |          |        |   | 1      | 1        |
|               | ٠<br>ک  | VESAGE  | V F 0                                    | ¥           |        |   |   |   |          | 1        |        | : | İ      | :        |
|               | # AX 1 40° A<br>29 - HS<br>- 25 9538<br>- 117 5 6 6 | FAXISUE AV                                    | 2 E O                                    | 200         |        |   |   |   |          | i        |        |   |        | <br>     |
|               | 20 1 10 10 10 10 10 10 10 10 10 10 10 10            | 202<br>24-<br>10                              |  |             | i      |   |   |   |          |          |        | - |        |          |
|               | × 0,-   | 7   | X 47                                     | 10.90       | 1      |   |   |   |          | Ì        |        | ì |        |          |
| 35            | †   | Ξ   | •  | 7           |        |   |   |   | 1        | 1        |        |   |        | !        |
| 43.50 HUUFS   | :<br>21 •25 •                                       | ci: •   | ikst<br>ikst                             | B           |        |   |   |   | <u> </u> |          | į      | j | · · ·  | ]<br>    |
| 97.           | 2   | 210.  | 368-74                                   | 4           |        |   |   |   |          | 1,       | 1      |   | !      | <u> </u> |
| 4             | <b>24</b> (1  | .   | 36                                       | AFCA        |        |   |   |   |          |          |        |   |        |          |
| يد.           | •   |   |  | 7           |        |   |   |   |          |          |        | İ |        |          |
| 1.1           | (5000)  |   |  | CUMULAT IVE |        |   |   |   |          | •        | į      | ì |        | !        |
| F .           | ي المالية   |   |  | 20          |        |   | }                                       |   |          | !        | İ      |   |        |          |
| •             | ::3   |   |  | ರ           |        |   |   |   |          |          | }      |   | 1      | !<br>!   |
| . 15 512      | :   | i   | į  |             |        |   |   |   |          | 1        |        |   |        |          |
| (4            | W-0   | ري<br>ناټو د                                  | 43.50                                    |             |        |   |   |   |          |          |        | - |        |          |
|               | 41.50   | 44. E. S. S. S. S. S. S. S. S. S. S. S. S. S. |  |             |        |   |   |   |          |          |        |   |        | !        |
| 5             | 9   | - (   | i  |             |        |   |   | 1 |          | 1        |        |   | !      | !        |
| เปรายน        |   | F STEP ACE 236.                               | 14 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | -           |        |   |   |   |          |          |        | 1 | 1      |          |
| 1             | 年の6<br>中で4<br>                                      | 1-1-1-1<br>1-1-1-1                            | 65 (A)<br>6- (A)<br>6- (A)<br>6- (A)     |             |        | 1 |   |   |          | 1        |        | 1 | !      | 1        |
| <u>۔</u><br>ء | 1000<br>1000<br>1000                                | 7'4<br>0.1'(1                                 | ار المراجعة<br>معاملة<br>المراجعة        | }           |        | İ |   |   |          |          |        | ! | !      | į        |

PEAK FLEG AND STAGE (EGG -3E-2PC) SUPERINGE BULLIFUE PLAN-KATID ECONOMIC COMPUTATIONS AREA IN SOUTHER BILES

| CFEETTICK        | STATICE    | * 13 '5 '4' | PLAN                                     | RATIO1   | FATIUS AFPLIED TO FLOWS |
|------------------|------------|-------------|--|--|-------------------------|
| EYDEÇ 68 APH- AT | : ¥        | 96°5        |  | 12000.   |                         |
| FCUTTO TO        | 24         | 66.3        | 1 6 5 4                                  | 11932  |                         |
|                  |            |             | STAC STAC                                | 1465 S 14 FFFT 119.53  |                         |
| RCCTED TO        | F 3        | 96*5        | 1 1103                                   | 11930.   |                         |
|                  |            |             | ** FLAN STAGE 11: 8 11: 8                | 46ES IN FUET<br>13.14<br>43.00   |                         |
| RECTED TO        | P 4        | 5.16        | 1 1168                                   | 11910.   |                         |
|                  |            |             |  | 3F-S- 1W FEET 15:01  | **                      |
|                  | A.         |             |  | 11597  |                         |
|                  |            |             | ** PEAK 51/0                             | 76F5 TN FUET<br>14-33  |                         |
| PYOP COPARM AT   | 2.6        | 6.30        | 1 51,64                                  | 15421  |                         |
| Z CCMEINED AT    |            | 10.90       | 1 110 E                                  | 21537.   |                         |
| FCUTE TO         | a <b>1</b> | 10.90       | 75 U 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 21554  |                         |
|                  |            |             | 1 5136<br>1 1136                         | 340 PER 340 PE |                         |

.

10P UF PAR 359.00 50.

SPILLBAY CREST 255,00

INITIAL VALUE

|   |                          |   |   |   |   | · |   |  |
|---|--------------------------|---|---|---|---|---|---|--|
| TINE OF<br>FAILURE<br>HOURS   | 0.00                     |   |   |   |   |   |   |  |
| COVERTION TIME OF TIME OF COVER TOP MAX CUTFLON FAILURE HOURS HOURS   | 00.54                    |   |   |   |   |   |   |  |
| CIVE TOP  | 00.01                    |   |   | • |   |   |   |  |
| OUTFLUN<br>COFFE  | • 60017                  |   |   |   | • |   |   |  |
| MAX IRU<br>STAX IRU<br>ACTAGE   | • 057                    | - |   |   |   |   | ٠ |  |
| MAXIFUN<br>DEPTH<br>CVFS FAM:-  | 11.0                     |   | , |   | • |   |   |  |
| 41.55 PM 3.55 | Cook                     |   |   |   |   |   | • |  |
| TITA A  | ** NCFMAL END OF JOL 908 |   |   | · |   |   |   |  |

APPENDIX 5

REFERENCES

BLAIR LAKE DAM

## APPENDIX 5 REFERENCES

## BLAIR LAKE DAM

Chow, Ven Te, Open Channel Hydraulics, McGraw Hill Book Company, New York, 1959.

King, H.W. and E.F. Brater, <u>Handbook of Hydraulics</u>, McGraw Hill Book Company, New York, Fifth Edition 1963.

Lewis, J.V. and H.B. Kummel (1910-1912) Geologic Map of New Jersey, revised by H.B. Kummel, 1931, and by M.E. Johnson, 1950. New Jersey Department of Conservation of Economic Development Atlas.

Salisbury, Kummel, Peet and Whitson, (1902) Glacial Map of New Jersey.

Schway, G.O., R.K. Frevert, T.W. Edmister, and K.K. Barnes, Soil and Water Conservation Engineering, The Ferguson Foundation Agricultural Engineering Series, John Wiley and Sons, Inc., New York, 1966, 683 pp.

Sharpe, John C. Memoirs of Blair, privately printed in Blairstown, N.J. 1939.

- U.S. Army Corps of Engineers, Hydrologic Engineering Center, Flood Hydrograph Package (HEC-1) Users Manual-Preliminary, Davis, California, March 1981.
- U.S. Department of Agriculture, Soil Conservation Service, Urban Hydrology for Small Watersheds, Technical Release No. 55, Washington, 1975.
- U.S. Department of Commerce, Weather Bureau, "Seasonal Variation of the Probable Maximum Precipitation East of the 105th Meridian for Areas from 10 to 1000 Square Miles and Durations of 6, 12, 24, and 48 Hours", Hydrometeorological Report No. 33, Washington, 1977, 816 pp.

United States Department of Interior, Bureau of Reclamation, Design of Small Dams, U.S. Government Printing Office, Washington, 1977, 816 pp.

U.S. Department of Interior, Geological Survey, 7.5-Minute Series (topographic) maps, scale 1:24000, Contour Interval 10 feet: Blairstown, New Jersey, (1955), Photorevised 1970.

Viessman, Warren, Jr., J.W. Knapp, G.L. Lewis, T.E. Harbaugh, Introduction to Hydrology, Harper and Row, Publishers, New York, Second Edition 1977, 704 pp.

